

THE APPLICATION OF EXTENDED  
KALMAN FILTERING TO THE  
POSITION LOCATING REPORTING SYSTEM (PLRS)

Charles A. Dittmar

MANUAL OF INFORMATION REPORTING SYSTEM

DUDLEY KNOX LIBRARY  
NAVAL POSTGRADUATE SCHOOL  
MONTEREY, CALIFORNIA 93940



# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

THE APPLICATION OF EXTENDED  
KALMAN FILTERING TO THE  
POSITION LOCATING REPORTING SYSTEM (PLRS)

by

Charles A. Dittmar, Jr.

December 1975

Thesis Advisor:

H.A. Titus

Approved for public release; distribution unlimited.

Prepared for:  
Naval Electronics System Command  
Washington, D.C. 22030

T173026

NAVAL POSTGRADUATE SCHOOL  
Monterey, California

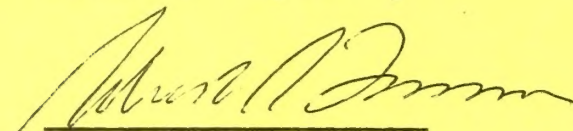
Rear Admiral Isham Linder  
Superintendent

Jack R. Borsting  
Provost

This thesis prepared in conjunction with research supported in part by Naval Electronics System Command under Project Number N0003975PO52945.

Reproduction of all or part of this report is authorized.

Released as a  
Technical Report by:

  
Dean of Research



REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NPS-52TS75121	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) The Application of Extended Kalman Filtering to the Position Locating Reporting System (PLRS)		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis; December 1975
7. AUTHOR(s) Charles A. Dittmar, Jr.		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE December 1975
		13. NUMBER OF PAGES 79
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES Research supported in part by Naval Electronics System Command under Project Number N0003975PO52945.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) PLRS Position Locating Reporting System Extended Kalman filtering		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Extended Kalman filtering is applied to the PLRS (Position Locating Reporting System). Here the nonlinearity to the filter enters through the measurement (range only). The nonlinearity being the relationship between range and the cartesian coordinate states of the filter. Filter covariances of error are portrayed as error ellipsoids. These are used to determine which one		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990	991	992	993	994	995	996	997	998	999	1000	1001	1002	1003	1004	1005	1006	1007	1008	1009	1010	1011	1012	1013	1014	1015	1016	1017	1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150	1151	1152	1153	1154	1155	1156	1157	1158	1159	1160	1161	1162	1163	1164	1165	1166	1167	1168	1169	1170	1171	1172	1173	1174	1175	1176	1177	1178	1179	1180	1181	1182	1183	1184	1185	1186	1187	1188	1189	1190	1191	1192	1193	1194	1195	1196	1197	1198	1199	1200	1201	1202	1203	1204	1205	1206	1207	1208	1209	1210	1211	1212	1213	1214	1215	1216	1217	1218	1219	1220	1221	1222	1223	1224	1225	1226	1227	1228	1229	1230	1231	1232	1233	1234	1235	1236	1237	1238	1239	1240	1241	1242	1243	1244	1245	1246	1247	1248	1249	1250	1251	1252	1253	1254	1255	1256	1257	1258	1259	1260	1261	1262	1263	1264	1265	1266	1267	1268	1269	1270	1271	1272	1273	1274	1275	1276	1277	1278	1279	1280	1281	1282	1283	1284	1285	1286	1287	1288	1289	1290	1291	1292	1293	1294	1295	1296	1297	1298	1299	1300	1301	1302	1303	1304	1305	1306	1307	1308	1309	1310	1311	1312	1313	1314	1315	1316	1317	1318	1319	1320	1321	1322	1323	1324	1325	1326	1327	1328	1329	1330	1331	1332	1333	1334	1335	1336	1337	1338	1339	1340	1341	1342	1343	1344	1345	1346	1347	1348	1349	1350	1351	1352	1353	1354	1355	1356	1357	1358	1359	1360	1361	1362	1363	1364	1365	1366	1367	1368	1369	1370	1371	1372	1373	1374	1375	1376	1377	1378	1379	1380	1381	1382	1383	1384	1385	1386	1387	1388	1389	1390	1391	1392	1393	1394	1395	1396	1397	1398	1399	1400	1401	1402	1403	1404	1405	1406	1407	1408	1409	1410	1411	1412	1413	1414	1415	1416	1417	1418	1419	1420	1421	1422	1423	1424	1425	1426	1427	1428	1429	1430	1431	1432	1433	1434	1435	1436	1437	1438	1439	1440	1441	1442	1443	1444	1445	1446	1447	1448	1449	1450	1451	1452	1453	1454	1455	1456	1457	1458	1459	1460	1461	1462	1463	1464	1465	1466	1467	1468	1469	1470	1471	1472	1473	1474	1475	1476	1477	1478	1479	1480	1481	1482	1483	1484	1485	1486	1487	1488	1489	1490	1491	1
---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	---



## (20. ABSTRACT Continued)

should be used to update a unit when there are several other units available for ranging. One should attempt to make the range measurement in the same direction as the major axis of error associated with the unit to be updated.

The filtering techniques are evaluated using static units and high speed maneuvering aircraft.





The Application of Extended Kalman Filtering to the  
Position Locating Reporting System(PLRS)

by

Charles A. Dittmar, Jr.  
Captain, United States Marine Corps  
B.S., United States Naval Academy, 1968

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL  
December 1975





## ABSTRACT

Extended Kalman filtering is applied to the PLRS (Position Locating Reporting System). Here the nonlinearity to the filter enters through the measurement (range only). The nonlinearity being the relationship between range and the cartesian coordinate states of the filter.

Filter covariances of error are portrayed as error ellipsoids. These are used to determine which one should be used to update a unit when there are several other units available for ranging. One should attempt to make the range measurement in the same direction of the major axis of error associated with the unit to be updated.

The filtering techniques are evaluated using static units and high speed maneuvering aircraft.





## TABLE OF CONTENTS

I.	INTRODUCTION -----	8
II.	POSITION LOCATING PROBLEM -----	11
	A. THE FILTER'S DYNAMIC MODEL OF AIRCRAFT UNITS -----	11
	B. EXTENDED KALMAN FILTER -----	12
III.	RANGE MEASUREMENT PROCESSING AND ERROR ELLIPSOIDS -----	17
IV.	TRACKING AND MANEUVERING TARGETS -----	26
	A. THE CHOICE OF $Q$ -----	26
	B. SIMULATION RESULTS -----	27
V.	CONCLUSIONS -----	39
	APPENDIX. COMPUTER PROGRAM -----	40
	LIST OF REFERENCES -----	78
	INITIAL DISTRIBUTION LIST -----	79





## LIST OF FIGURES

1. Error ellipsoids for two fixed units displaced along y-axis 15 KM ----- 20
2. Projection of error ellipsoids to their x-y components and updated error ellipsoids after each unit ranges on the other ----- 21
3. Sequential updating of the units, one upon the other, over ten observations ----- 25
4. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging only on unit #2.  
x = true track,  $\square$  = noise track, + = filter track -- 31
5. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging on unit #2 and unit #1 during second half.  
x = true track,  $\square$  = noise track, + = filter track -- 32
6. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working poorly in last third of flight (unit #1 ranges solely on last 20 observations. A too low Q is indicated by the track bias.  
x = true track,  $\square$  = noise track, + = filter track -- 33
7. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 10 M.  
x = true track,  $\square$  = noise track, + = filter track -- 34
8. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 100 M.  
x = true track,  $\square$  = noise track, + = filter track -- 35
9. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Filter drops track due to extreme measurement noise (1 KM).  
x = true track,  $\square$  = noise track, + = filter track -- 36





10. Aircraft in circular track at Mach 1 and radius of 10 KM. Error ellipsoids presented on every fifth observation. Measurement noise = 10 M. Switching algorithm fails on x-axis. Ellipses 25 times true scale.  
x = true track,  $\square$  = noise track, + = filter track -- 37
11. Aircraft in circular track at Mach 1 and radius of 10 KM. Switching algorithm corrected. Ellipses 25 times true scale.  
x = true track,  $\square$  = noise track, + = filter track -- 38



## I. INTRODUCTION

Position location of tactical elements in the Marine Corps in the past has relied upon the fact that these units had maps from which they could determine their position. Position determination is therefore highly dependent on the ability of an individual to correctly orient himself to the natural terrain surrounding him and locate this same terrain on the map. Once located, the requirement then exists to transmit position information via radio link to parent units. Meshed with the ground commander's problem of position location is the task of organizing and conducting support operations such as medical evacuation of wounded personnel, artillery, naval gunfire and air support.

Using visual references it becomes difficult to accurately locate one's position when operating in mountainous terrain, in heavy vegetation, at night or in bad weather. And with the heavy volume of radio traffic experienced during battle, the probability of communicating to higher headquarters a unit's position or information about that position is reduced. As a result the support operations mentioned earlier are delayed because of detailed clearances required to ensure protection of friendly units whose position is not precisely known.

The obstacles to position location suggested can and do arise in the conduct of actual operations, and for that





reason, the Marine Corps has written specifications detailing a Position Location and Reporting System (PLRS) designed for tactical employment on the battlefield, [1]. The system as construed is to consist of a containerized master unit composed of a general purpose computer and communications control electronics. This unit is referred to as the Master Unit. It is responsible for processing all range information inputs to the system, and displaying unit positions on a visual display with a variety of other information.

The other units in the area are all portable, capable of being carried by a single man, vehicle, or aircraft. They are referred to as update or ranging units depending on their particular function at the time. When a unit's position is being improved, that unit is referred to as the "update" unit. All other units that are in contact with the update unit and are providing range measurements are "ranging" units. The frequency at which each unit is updated is specified according to its type. That is, aircraft traveling at much higher velocities than men will require updates more often if their tracking is to be accurate.

Before a unit can be tracked and position estimates made, an initial estimate of position must be made. This process of initialization is controlled by the master unit. Once a unit is initialized the computer systematically selects ranging units processing their associated range information as applicable. In processing range information a new position estimate and a measure of the uncertainty in the estimate is provided.





While the processing of accumulated range information for an update unit appears to be straightforward, the difficulty lies in deciding which ranges to process so that the most accurate position estimates will be obtained. Range information is a measurement of the time required to send a signal from the ranging unit to the update unit and back again plus some built in delays.

While the measurement of times associated with the total time is quite accurate, it is still subject to the effects of noise therefore range is a noisy measurement. In addition the uncertainty of the ranging unit's position adds to the uncertainty of the measurement itself. Therefore the selection of a ranging unit to best update a particular unit becomes a very important factor in the position location problem. One would desire to use the ranging unit nearest the line of the major axis of error in the unit to be updated.

The error ellipsoids of the "update" and "ranging" units and their relative geometry are analyzed and their influence on the tracking is portrayed in examples with maneuvering high speed aircraft and with stationary units.



## II. POSITION LOCATING PROBLEM

### A. THE FILTER'S DYNAMIC MODEL OF AIRCRAFT UNITS

First consider units in aircraft in a two dimensional space.\* The estimate that we seek in this problem is position  $(X,Y)$  and velocity,  $(\dot{X},\dot{Y})$ .  $X$  and  $Y$  are calculated with respect to a relative grid at a point on the earth's surface. The altitude is the vertical height above the earth at that particular  $XY$  grid intersection, and is not utilized in this investigation.

For tracking we may choose a fourth order state vector,

$$\underline{x} = \begin{bmatrix} X \\ \dot{X} \\ Y \\ \dot{Y} \end{bmatrix} \quad (1)$$

Writing the equations in linear state form results in

$$\underline{x}(k+1) = \Phi \underline{x}(k) + \Gamma \underline{w}(k) \quad (2)$$

where

$$\Phi = \begin{bmatrix} 1 & T & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & T \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (3)$$

---

\*The altitude tracking will be handled independently.





and

$$\Gamma = \begin{bmatrix} \frac{T^2}{2} & 0 \\ T & 0 \\ 0 & \frac{T^2}{2} \\ 0 & T \end{bmatrix} \quad (4)$$

## B. EXTENDED KALMAN FILTER

The observable range is a nonlinear function of the states. So we must briefly look at how the nonlinearities can be handled in this type of problem.

Consider a nonlinear discrete system of state and observation equations given by

$$\underline{x}(k+1) = \underline{f}(\underline{x}(k), k) + \underline{g}(\underline{x}(k), k) \cdot \underline{w}(k) \quad (5)$$

and

$$\underline{z}(k) = \underline{h}(\underline{x}(k), k) + \underline{v}(k) \quad (6)$$

In these equations  $\underline{f}$ ,  $\underline{g}$  and  $\underline{h}$  are nonlinear functions of the state variables  $\underline{x}$ ,  $\underline{w}(k)$  is plant excitation noise, and  $\underline{v}(k)$  is measurement noise. The plant noise and measurement noise are assumed uncorrelated, zero-mean, and white. That is



$$E[\underline{w}(k) \cdot \underline{w}^T(j)] = Q'(k) \delta_{kj}$$

and

$$E[\underline{v}(k) \cdot \underline{v}^T(j)] = R(k) \delta_{kj}$$

In order to apply the linear filter equations, (5) and (6) are expanded about the best estimate of the state at that time and only the first-order terms are kept. Equation (5) gives

$$\underline{x}(k+1) = \Phi(k) \underline{x}(k) + \Gamma(k) \cdot \underline{w}(k) , \quad (7)$$

with

$$\Phi(k) = \left. \frac{\partial \underline{f}}{\partial \underline{x}} \right|_{\underline{x}=\hat{\underline{x}}(k)} .$$

Similarly Eq. (6) yields

$$\underline{z}(k) = H(k) \underline{x}(k) + \underline{v}(k) \quad (8)$$

where

$$H(k) = \left. \frac{\partial \underline{h}}{\partial \underline{x}} \right|_{\underline{x}=\underline{x}'(k)} . \quad (9)$$

$\hat{\underline{x}}(k)$  is the estimated state value after the  $k^{\text{th}}$  measurement and  $\underline{x}'(k)$  is the predicted value of the state before the  $k^{\text{th}}$  measurement. That is,





$$\underline{x}'(k) = \underline{f}(\underline{\hat{x}}(k-1), k-1) . \quad (10)$$

A state error vector is defined by

$$\underline{\tilde{x}}(k) = \underline{\hat{x}}(k) - \underline{x}(k) ,$$

and a predicted state error vector is defined by

$$\underline{\tilde{x}}'(k) = \underline{x}'(k) - \underline{x}(k) .$$

The covariance of state error matrix is defined by

$$P(k) = E[\underline{\tilde{x}}(k) \cdot \underline{\tilde{x}}^T(k)] ,$$

and the predicted covariance of state error matrix is given by

$$P'(k) = E[\underline{\tilde{x}}'(k) \cdot \underline{\tilde{x}}'^T(k)] .$$

The state excitation matrix is given by

$$Q(k) = E[\Gamma(k) \cdot \underline{w}(k) \cdot \underline{w}^T(k) \cdot \Gamma^T(k)] ,$$

and the measurement noise covariance matrix is

$$R(k) = E[\underline{v}(k) \cdot \underline{v}^T(k)] .$$



The Kalman Filter equations are given by [2]

$$P'(k+1) = \Phi(k)P(k)\Phi^T(k) + Q(k) \quad (11)$$

$$G(k) = P'(k)H^T(k) [H(k)P'(k)H^T(k) + R(k)]^{-1} \quad (12)$$

$$P(k) = [I - G(k)H(k)] P'(k) \quad (13)$$

$$\underline{x}'(k) = \underline{f}(\hat{\underline{x}}(k-1), k) \quad (14)$$

$$\underline{z}'(k) = \underline{h}(\underline{x}'(k), k) \quad (15)$$

$$\hat{\underline{x}}(k) = \underline{x}'(k) + G(k) [\underline{z}(k) - \underline{z}'(k)] \quad (16)$$

The Q matrix serves not only to allow for maneuvering but also to account for any model inaccuracies. That is, any discrepancies between the true action of the physical system and its characterization by Eq. (7). For a filter which reaches steady-state conditions the Q also serves to prevent the gain matrix G(k) from approaching zero by always insuring uncertainty in the predicted covariance of error matrix P'(k).

The observation equation is nonlinear in the states and is given by

$$z(k) = [x(k)^2 + y(k)^2]^{1/2} \quad (17)$$





Equation (9) can be used to give observation matrix. The result is

$$H(k) = \begin{bmatrix} \frac{x(k)}{x(k)^2 + y(k)^2} & 0 & \frac{y(k)}{x(k)^2 + y(k)^2} & 0 \end{bmatrix} \quad (18)$$

In doing this, the recursive Kalman filter equations have been extended to cover the nonlinear case. The pseudo measurement matrix,  $H$ , must now be calculated from the position estimates at each time interval.

The use of the Extended Kalman technique in tracking a unit as it moves through the area presents a unique problem. Because we are observing only the range, we can improve our estimate of location only along the direction of the range vector. That is, the uncertainty or error variance in location remains unchanged in cross-range. We must then choose another ranging unit nearby that will improve upon this cross range error. This however is done later at the next prescribed interval for update of the unit in question.

The conclusion drawn from this observation is that it is critical that an algorithm be developed for selecting the best observations (ranging units) to process in the updating of a unit. It will be shown that this algorithm must be dependent on the physical geometry associated with the covariance error ellipses. It takes into consideration the error covariances associated with both the update and ranging units.



### III. RANGE MEASUREMENT PROCESSING AND ERROR ELLIPSOIDS

The position of each unit within the system is established with a degree of uncertainty about the estimate. This uncertainty is expressed in the covariance of error matrix,  $P$ , and represents the sigma squared error deviation about the estimate. The position diagonal terms ( $P_{11}$  and  $P_{33}$ ) of the covariance matrix represent the variances of the estimate in the XY coordinate directions. Their respective off diagonal terms (covariances) represent the degree of coupling and the orientation of the uncertainty in the XY plane.

If the errors were normally distributed, there exists a rotated coordinate system such that in the new system the orthogonal position components are uncorrelated. This is equivalent to taking the exponent of the joint normal probability density function, and applying a coordinate transformation which eliminates the cross terms.

The exponent (for zero-mean random variables) is

$$\frac{x^2}{\sigma_x^2} - \frac{2r_{xy}xy}{\sigma_x\sigma_y} + \frac{y^2}{\sigma_y^2} \quad . \quad (19)$$

When set equal to a constant, this curve, which is an ellipse, is a curve of constant probability. This ellipse does not have its major and minor axes aligned with the coordinate system however. By applying the transformation





$$x' = x \cos \theta + y \sin \theta \quad (20)$$

and

$$y' = y \cos \theta - x \sin \theta \quad (21)$$

with

$$\theta = \frac{1}{2} \tan^{-1} \left[ \frac{2 \frac{\text{cov}(x,y)}{2}}{\sigma_x^2 - \sigma_y^2} \right], \quad (22)$$

the ellipse will be aligned with the  $x'$ ,  $y'$  axis and the resultant random variables will be uncorrelated. The new variances in this system are calculated by

$$\sigma_{x'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} + \frac{\text{cov}(xy)}{\sin 2\theta}, \quad (23)$$

and

$$\sigma_{y'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} - \frac{\text{cov}(xy)}{\sin 2\theta}. \quad (24)$$

This method of viewing the sample statistics provides insight into the filter performance because it shows the regions of high probability and their geometric relationships. The values of  $\sigma_{x'}^2$  and  $\sigma_{y'}^2$  are referred to as the rotated error variances in the following section.



When a range measurement is made between two units, each with a different and independent error ellipse, the uncertainty of position along the range line connecting the two is improved for both units. In addition, it is sometimes possible to reduce the error of the axis orthogonal to the range line depending on the orientation of the error ellipse.

To study the influence of the error ellipsoids of the ranging and update unit let us consider a static example. This model is synonymous with those used for foot soldiers.

Measurement noise will be considered to come solely from the error variance of the ranging unit and vice versa when their roles interchanged. That is, at the same time the "update" unit is being updated, let us also update the "ranging" unit. The estimates of position and their error ellipsoids are shown in Fig. 1.

A projection of the error ellipsoid along the y-axis is given in Fig. 2. If one utilizes each as an observation to update the other, the resulting variance of both along the range line is given by

$$\sigma_{\text{new}}^2 = \frac{\sigma_1^2 \sigma_2^2}{\sigma_1^2 + \sigma_2^2}$$

where  $\sigma_1$  and  $\sigma_2$  are the standard deviations of units 1 and 2 in the range projection and  $\sigma_{\text{new}}$  is the new updated standard deviation for both units in the range projection ( $\sigma_y$ ), as is seen also in Fig. 2.





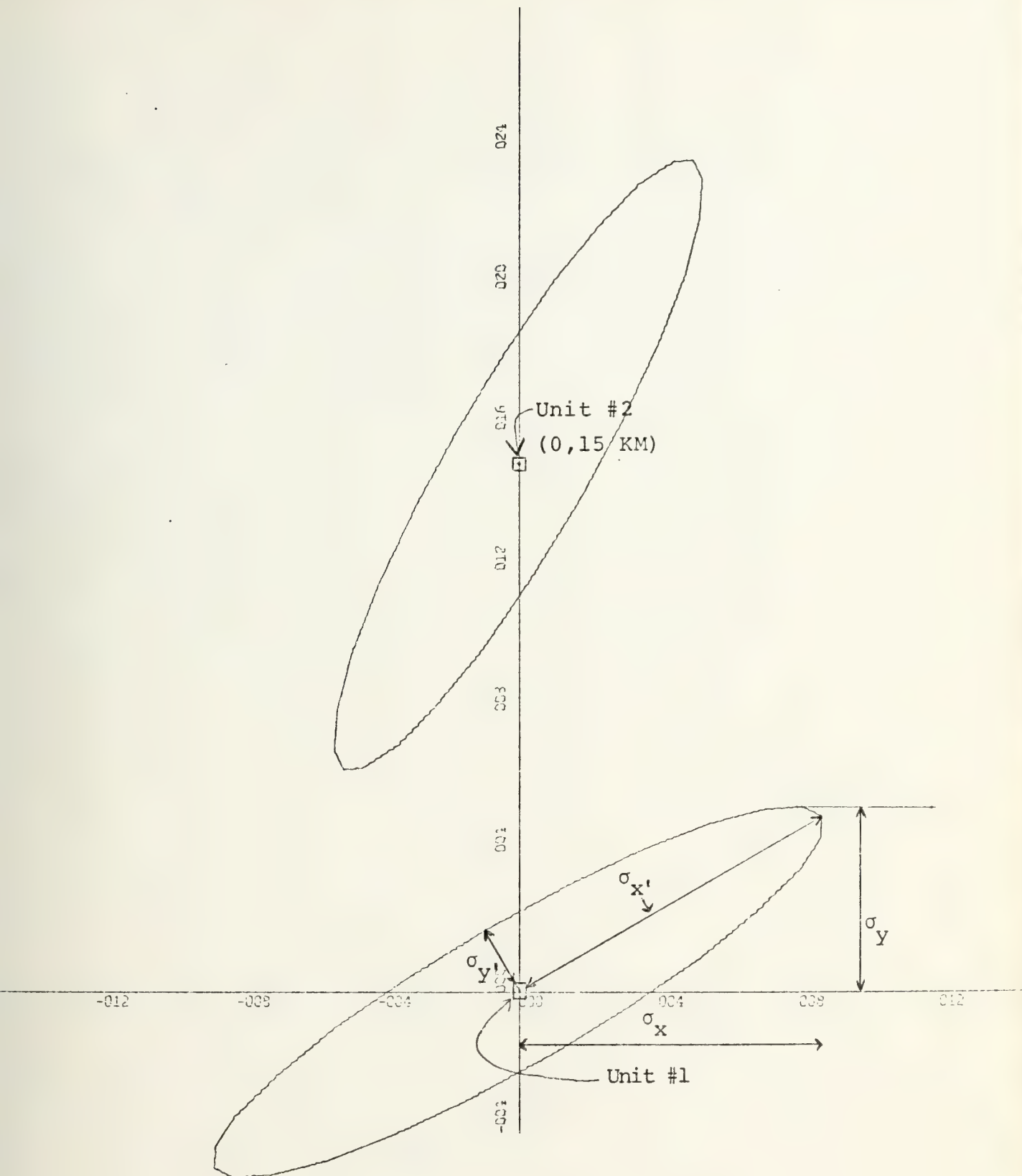


FIGURE 1. Error ellipsoids for two fixed units displaced along y-axis 15 KM



$$P_1 = \begin{bmatrix} 28 & 41.52 \\ 41.52 & 76 \end{bmatrix}$$

$$= \begin{bmatrix} \sigma_x^2 & \sigma_x \sigma_y \\ \sigma_x \sigma_y & \sigma_y^2 \end{bmatrix}$$

$$P_2 = \begin{bmatrix} 76 & 41.52 \\ 41.52 & 28 \end{bmatrix}$$

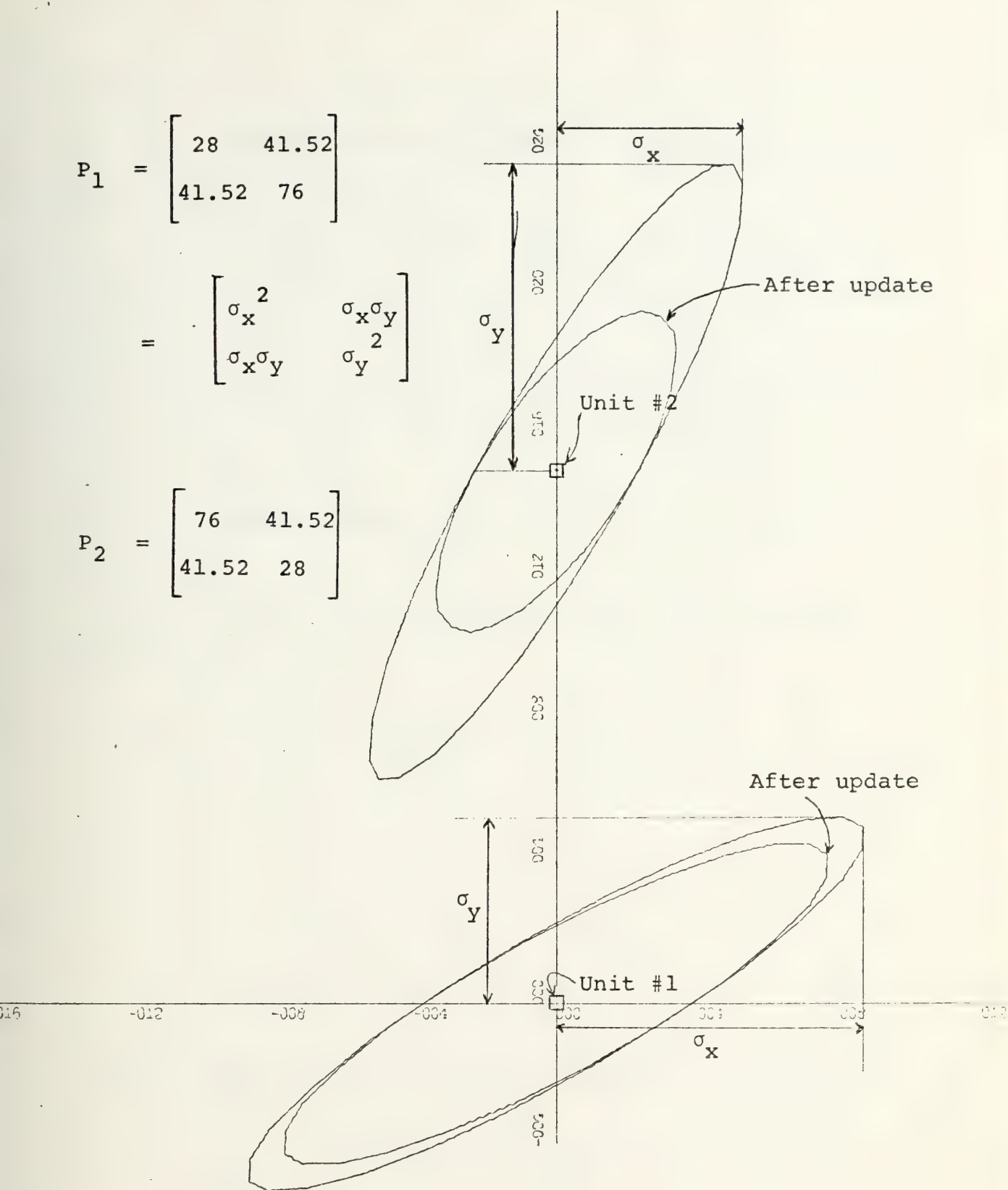


FIGURE 2. Projection of error ellipsoids to their x-y components and updated error ellipsoids after each unit ranges on the other





Thus the processing of an error free measurement between two units provides a better statistical description of both units along the range line.

This discussion considered fixed units with no velocity and only in the XY plane. Central to the equations employed in the Kalman filter are equations calculating the gains and the error covariance matrix. By merely adding the component of the variance of the ranging unit along the range line to the measurement noise in the calculation of the Kalman gains, the Kalman filter reduces the covariance matrix of the update unit properly.

The uncoupled error matrices and their directions are (from eqs. (22)-(24))

$$P_1' = \begin{bmatrix} 4 & 0 \\ 0 & 100 \end{bmatrix}, \quad \theta_1 = -30^\circ$$

and

$$P_2' = \begin{bmatrix} 100 & 0 \\ 0 & 4 \end{bmatrix}, \quad \theta_2 = +30^\circ$$

After update the resulting covariances are (see Fig. 2)

$$P_1(\text{new}) = \begin{bmatrix} 11.42 & 11.18 \\ 11.18 & 20.46 \end{bmatrix}$$



and

$$P_2(\text{new}) = \begin{bmatrix} 59.42 & 30.34 \\ 30.34 & 20.46 \end{bmatrix}$$

Their uncoupled equivalents

$$P_1'(\text{new}) = \begin{bmatrix} 3.89 & 0 \\ 0 & 28 \end{bmatrix}, \quad \theta_1(\text{new}) = -34^\circ$$

and

$$P_2'(\text{new}) = \begin{bmatrix} 7.6 & 0 \\ 0 & 3.89 \end{bmatrix}, \quad \theta_2(\text{new}) = 28.6^\circ$$

After ten updating operations

$$P_1(\text{new}) = \begin{bmatrix} 5.33 & 0.02 \\ 0.02 & 0.04 \end{bmatrix},$$

$$P_2'(\text{new}) = \begin{bmatrix} 14.52 & 0.06 \\ .06 & 0.04 \end{bmatrix}$$

and their uncoupled equivalents

$$P_1'(\text{new}) = \begin{bmatrix} 5.34 & 0 \\ 0 & .08 \end{bmatrix}, \quad \theta_1'(\text{new}) = 0.47^\circ$$



$$P_2' = \begin{bmatrix} 14.6 & 0 \\ 0 & .079 \end{bmatrix}, \quad \theta_2'(\text{new}) = 0.46^\circ$$

In Fig. 3 we see the influence of the sequential updating of the units, one upon the other over ten observations.

Note that the successive ranging in the y-direction effectively reduced the error variance in y and its projection in x due to the xy covariance. This was accomplished by assuming the measurement noise consists solely of the y component of the error variance of the other unit ranging upon it.





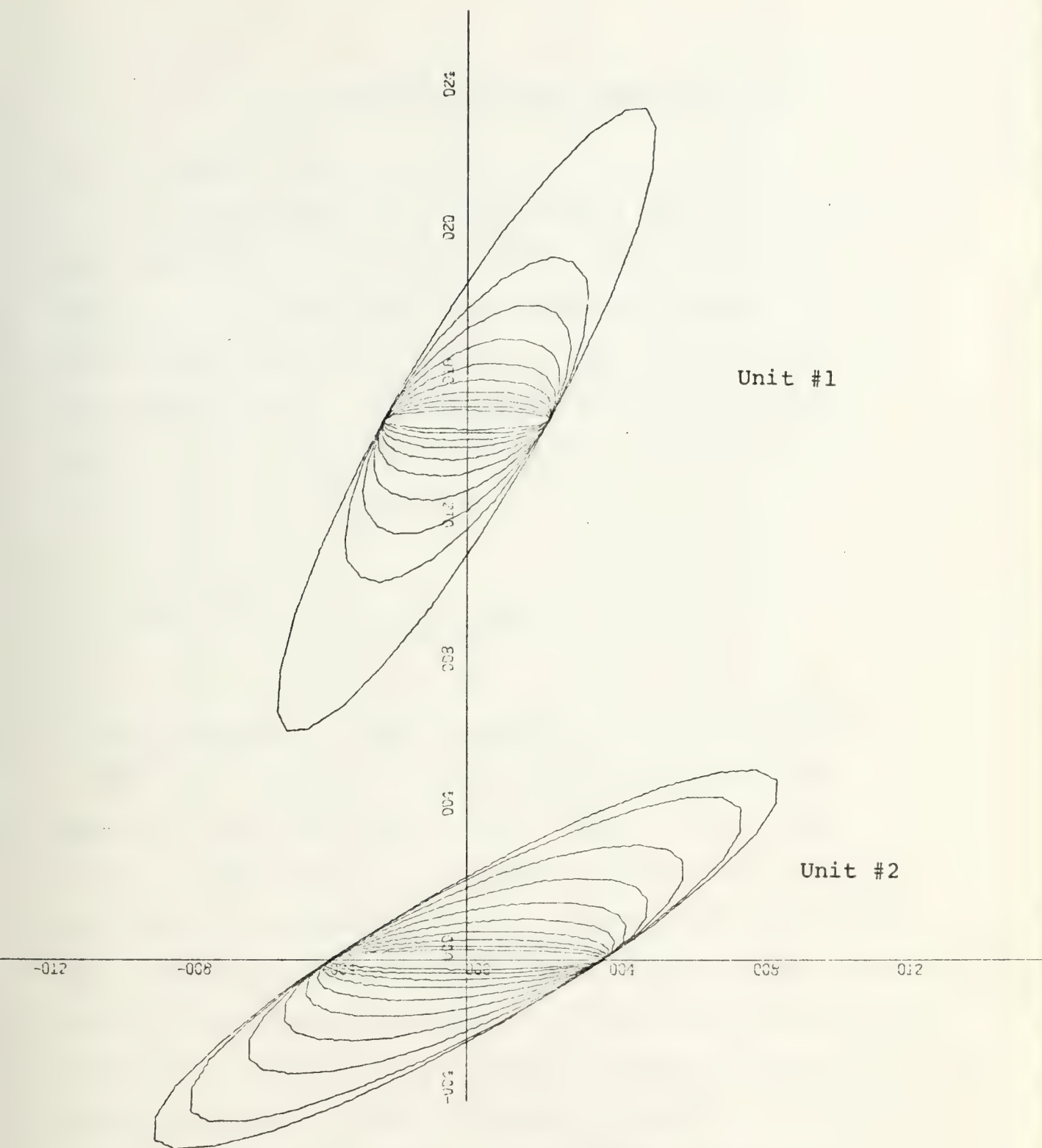


FIGURE 3. Sequential updating of the units, one upon the other, over ten observations



#### IV. TRACKING AND MANEUVERING TARGETS

##### A. THE CHOICE OF Q

One possible approach in designing a filter to accomodate maneuvers is to increase the random forcing excitation covariance,  $Q$ , until the filter adequately tracks the contemplated maneuvers. Normally this is done in a tracking simulation program. The running filter error residual,  $(\underline{x}(k) - \hat{\underline{x}}(k/k))$  appears to be a better indicator of effectiveness than either mean error

$$\text{Mean Error} = \frac{1}{k} \sum_{j=1}^k (\underline{x}(j) - \hat{\underline{x}}(j/j))$$

or for that matter, error variance. Filter lag or bias as is best seen in the sign of the error, is lost in the squaring process for the variance. Also, the mean and variance error entail an accumulation of all error from start up to the present time. In a simulation, a maneuver may often not occur until well into a tracking run, and its effect may not appear as markedly in the mean error and error variance. A Monte Carlo simulation is often an effective design tool here. However, unless considerable engineering insight is used the resulting filter has been designed to handle the zero mean maneuver. That is, the filter will be designed against an ensemble of maneuvering tracks the mean of which is no maneuver at all. It appears that a more





successful procedure is to design against a highly probable worst case maneuver. The resulting filter should then be able to handle all possible contingencies, which is a necessary ingredient in most military systems.

The price paid in having a rather high  $Q$  in a filter design is an increased degradation in filter performance due to the measurement noise variance,  $R$ . In this application the measurement noise is minimal. The important thing is to attempt range measurements along the axis of maximum filter error variance as discussed in Section III.

## B. SIMULATION RESULTS

An aircraft flying at Mach 1 follows a turn of radius 10 KM. Ranging unit 1 is located at the origin. Unit 2 is placed at (10 KM, 10 KM). We have the below filter parameters for Figs. 4 through 11 are

$$\Phi = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$$\Gamma = \begin{bmatrix} 0.5 & 0 \\ 1 & 0 \\ 0 & 0.5 \\ 0 & 1 \end{bmatrix}$$



and the initial conditions of

$$P(1/0) = \begin{bmatrix} 10^{-4} & 0 & 0 & 0 \\ 0 & 10^{-4} & 0 & 0 \\ 0 & 0 & 10^{-4} & 0 \\ 0 & 0 & 0 & 10^{-4} \end{bmatrix}$$

and

$$\underline{X}(1) = X(1/0) = \begin{bmatrix} 0 \\ 0.333 \text{ KM/S} \\ 10 \text{ KM} \\ 0 \end{bmatrix}$$

In Fig. 4 we have the first attempt at the algorithm for choosing the ranging unit nearest the line generated from the major axis of error in the error ellipsoid of the tracker. It ranged solely on unit 2 and failed to follow the turn. Similarly in Fig. 5, the filter ranged on unit 2 for the first half of the flight and on unit 1 for the second half.

The evolution of the design of the filter is presented here so that the errors in the design process may help to give insight into the filter's performance.

In Fig. 6 we see the beginning of proper functioning of the ranging algorithm (except on the last 20 observations). Note also that the covariance of excitation,  $Q$ , is insufficient to follow the maneuver as is indicated by the bias



in the filter track from the true track. Here we have

$$q_{11}/R = 2.5 \times 10^{-4}$$

from

$$R = 0.1$$

and

$$Q = \begin{bmatrix} .25 \times 10^{-4} & .5 \times 10^{-4} & 0 & 0 \\ .5 \times 10^{-4} & 1 \times 10^{-4} & 0 & 0 \\ 0 & 0 & .25 \times 10^{-4} & .5 \times 10^{-4} \\ 0 & 0 & .5 \times 10^{-4} & 1 \times 10^{-4} \end{bmatrix}$$

In Fig. 7 the algorithm appears to be functioning properly and there is sufficient  $Q$  for the filter to follow the turn. Here we have

$$q_{11}/R = 0.25$$

In Fig. 8 the filter was tested for its response to increasing the measurement noise (from  $\sigma_v = 0.01$  KM to  $\sigma_v = 0.1$  KM). It tracked well. However in Fig. 9, when the noise was again increased ( $\sigma_v = 1$  KM) the track was lost immediately. This gives one a ball-park indication of filter performance as the ranging observations are degraded.





Figure 10 shows the filter performance with the error ellipsoids superimposed at every fifth observation. It indicates a short malfunction of the switching algorithm when the track crosses the x-axis. This was corrected in Fig. 11. The error ellipsoids are expanded to twenty-five times their true value in order that they may be seen.

In the appendix we have listed the computer simulation program with comments regarding its operation.



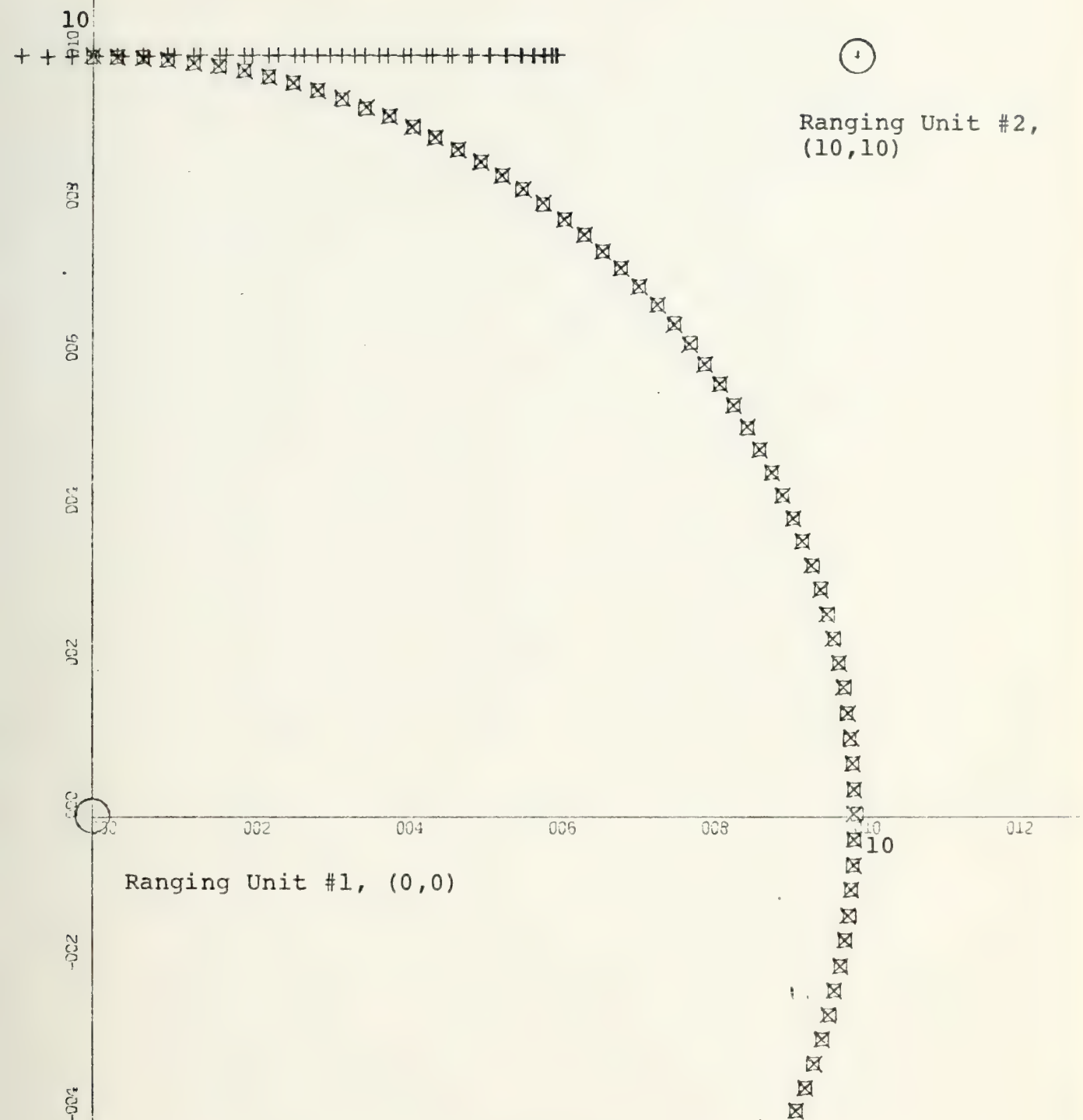


FIGURE 4. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging only on unit #2.  
 x = true track, O = noise track, + = filter track



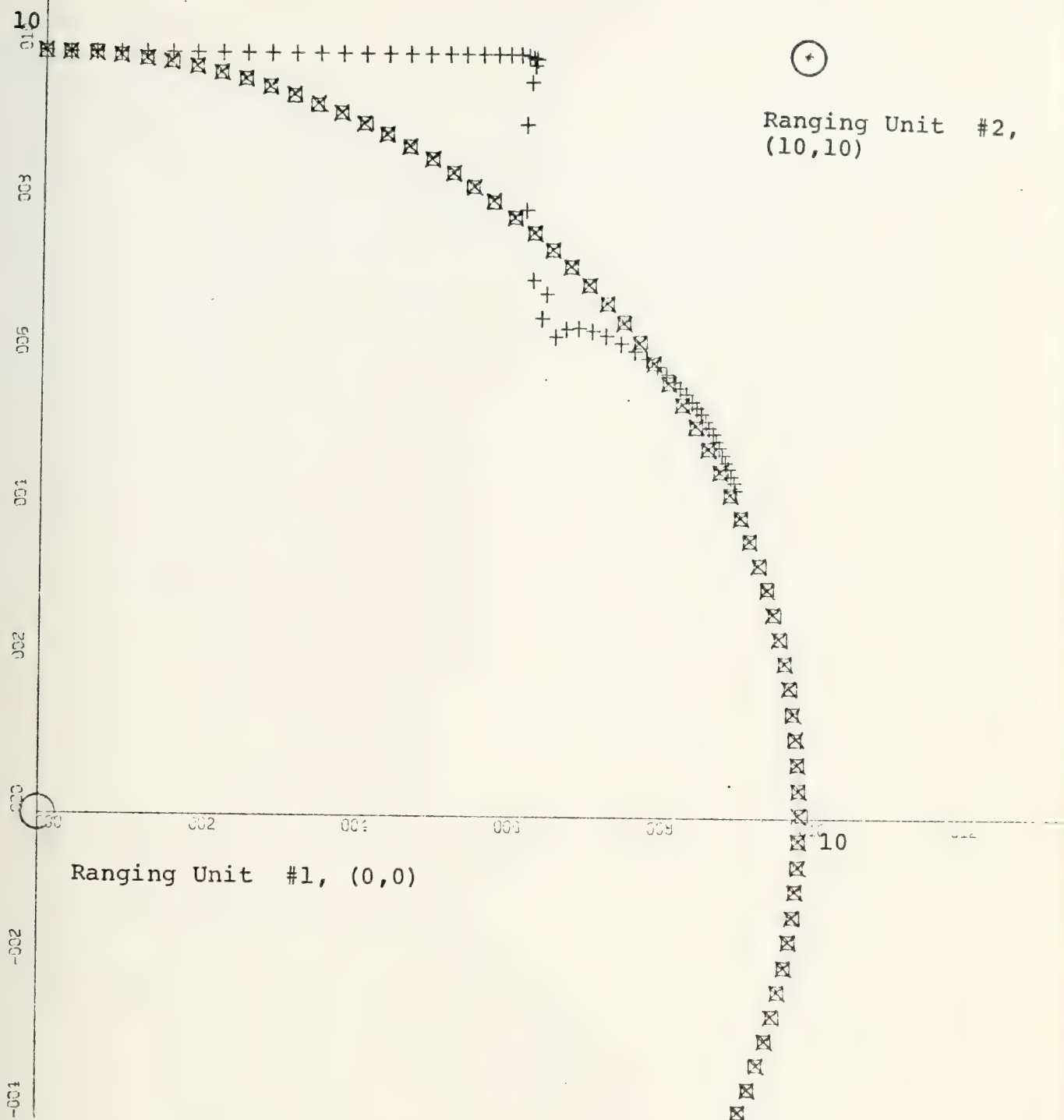


FIGURE 5. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging on unit #2 and unit #1 during second half.  
 x = true track, o = noise track, + = filter track





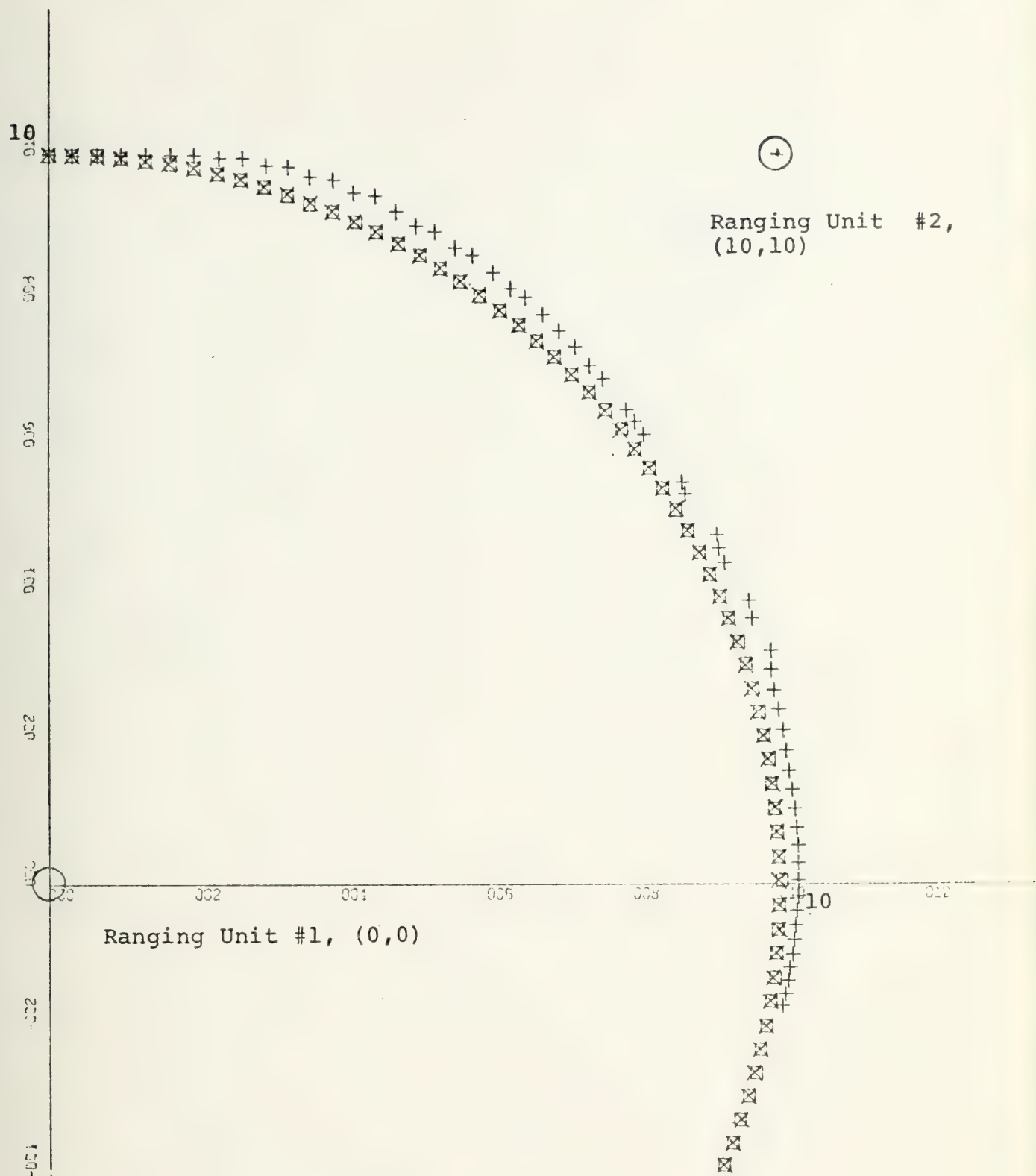


FIGURE 6. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working poorly in last third of flight (unit #1 ranges solely on last 20 observations. A too low  $Q$  is indicated by the track bias.  
 $x$  = true track,  $o$  = noise track,  $+$  = filter track



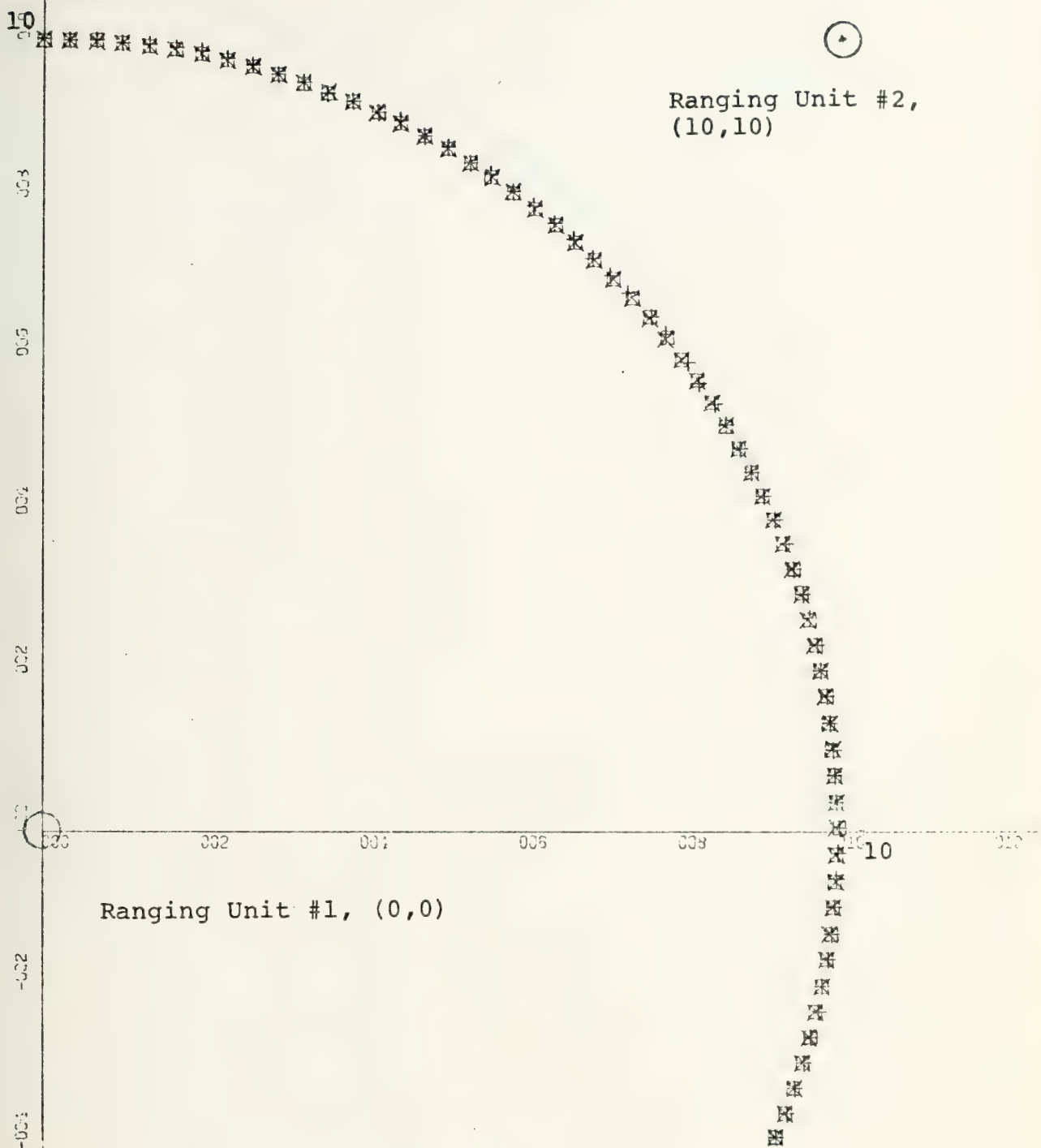


FIGURE 7. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working.  $Q$  sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 10 M.  
 $x$  = true track,  $o$  = noise track,  $+$  = filter track



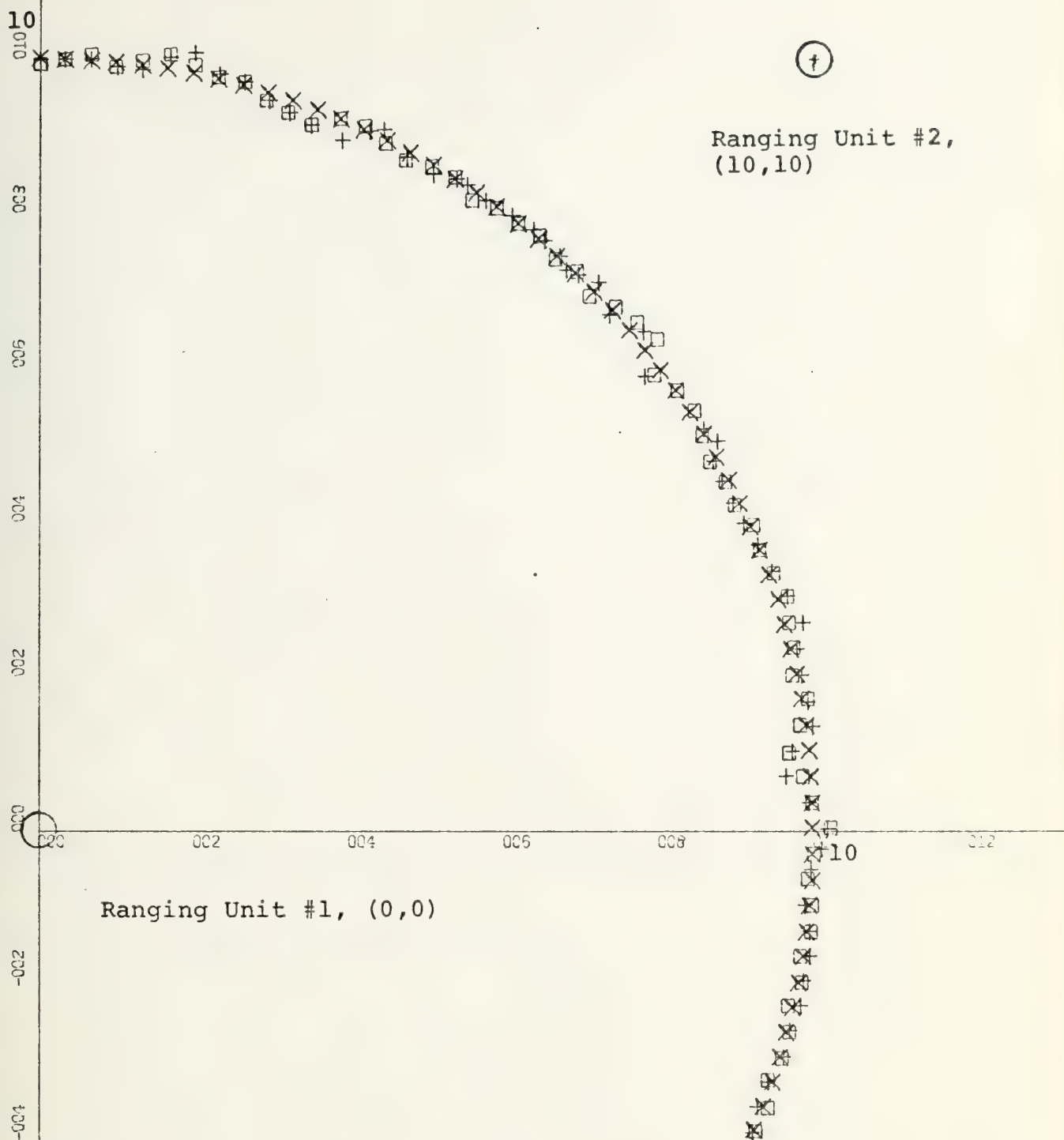


FIGURE 8. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working.  $Q$  sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 100 M.  
 $x$  = true track,  $o$  = noise track,  $+$  = filter track





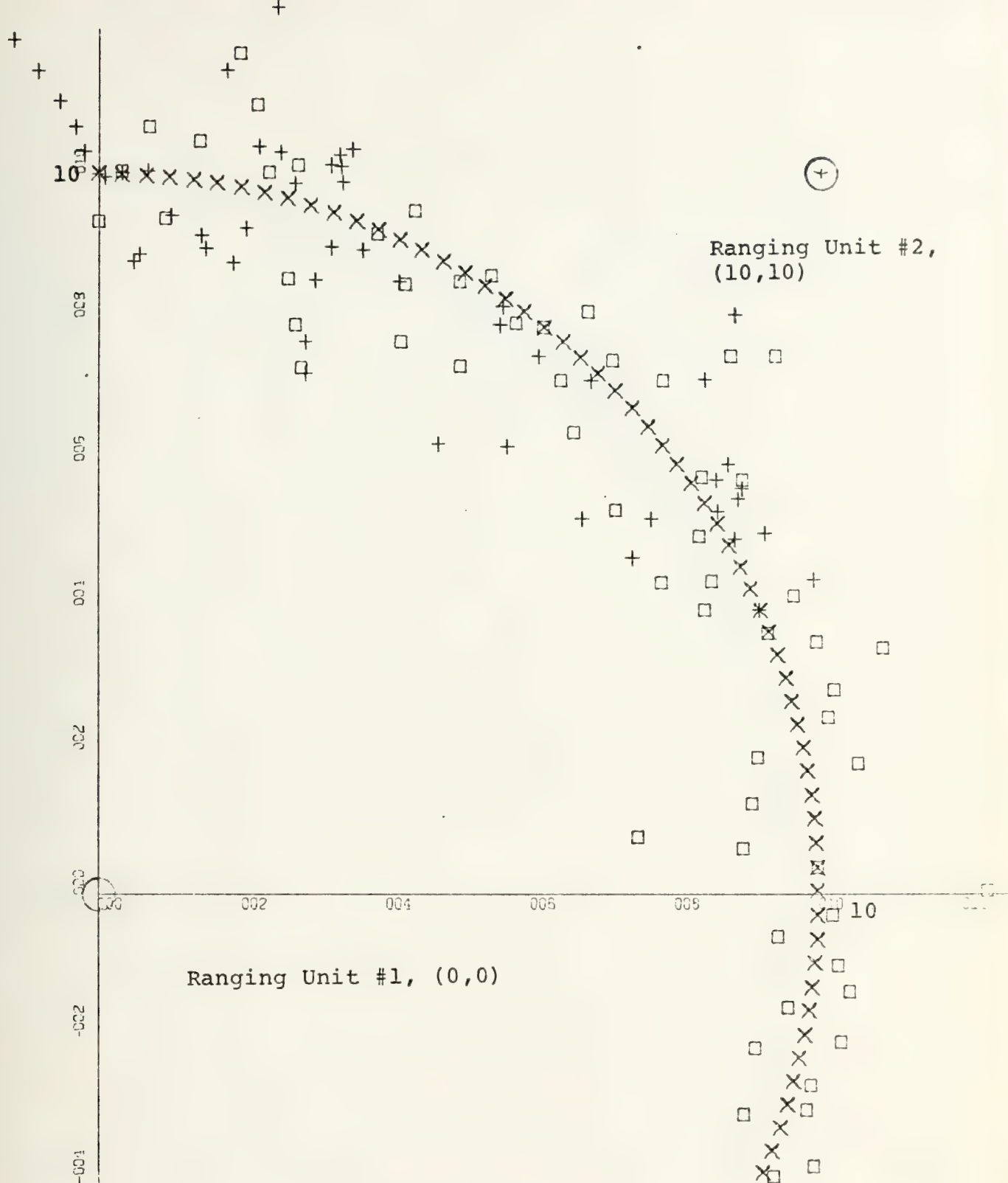


FIGURE 9. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Filter drops track. Measurement noise = 1 KM. x = true track, o = noise track, + = filter track



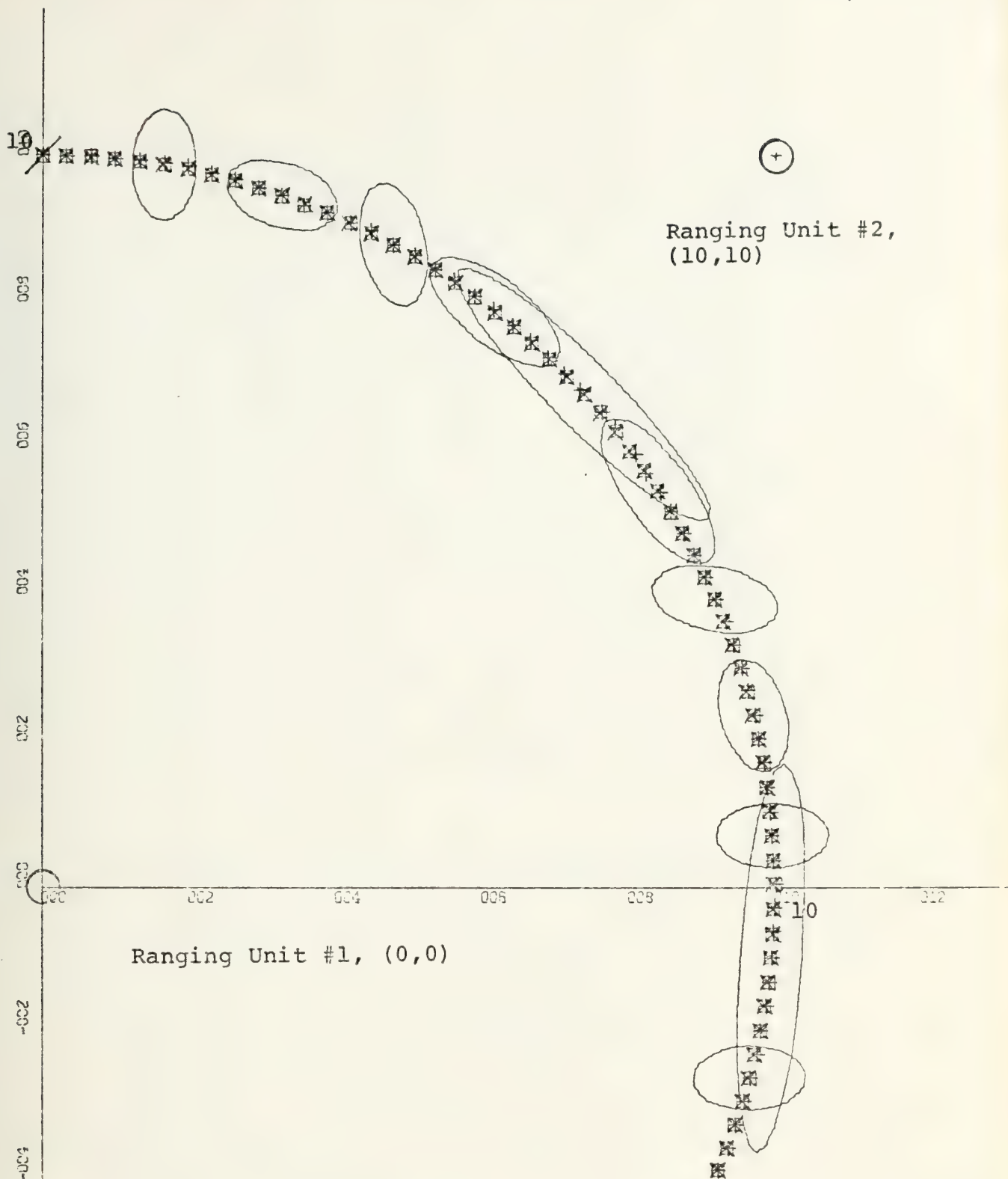


FIGURE 10. Aircraft in circular track at Mach 1 and radius of 10 KM. Error ellipsoids presented on every fifth observation. Measurement noise = 10 M. Switching algorithm fails on x-axis. Ellipses 25 times true scale.  
 x = true track,  $\square$  = noise track, + = filter track



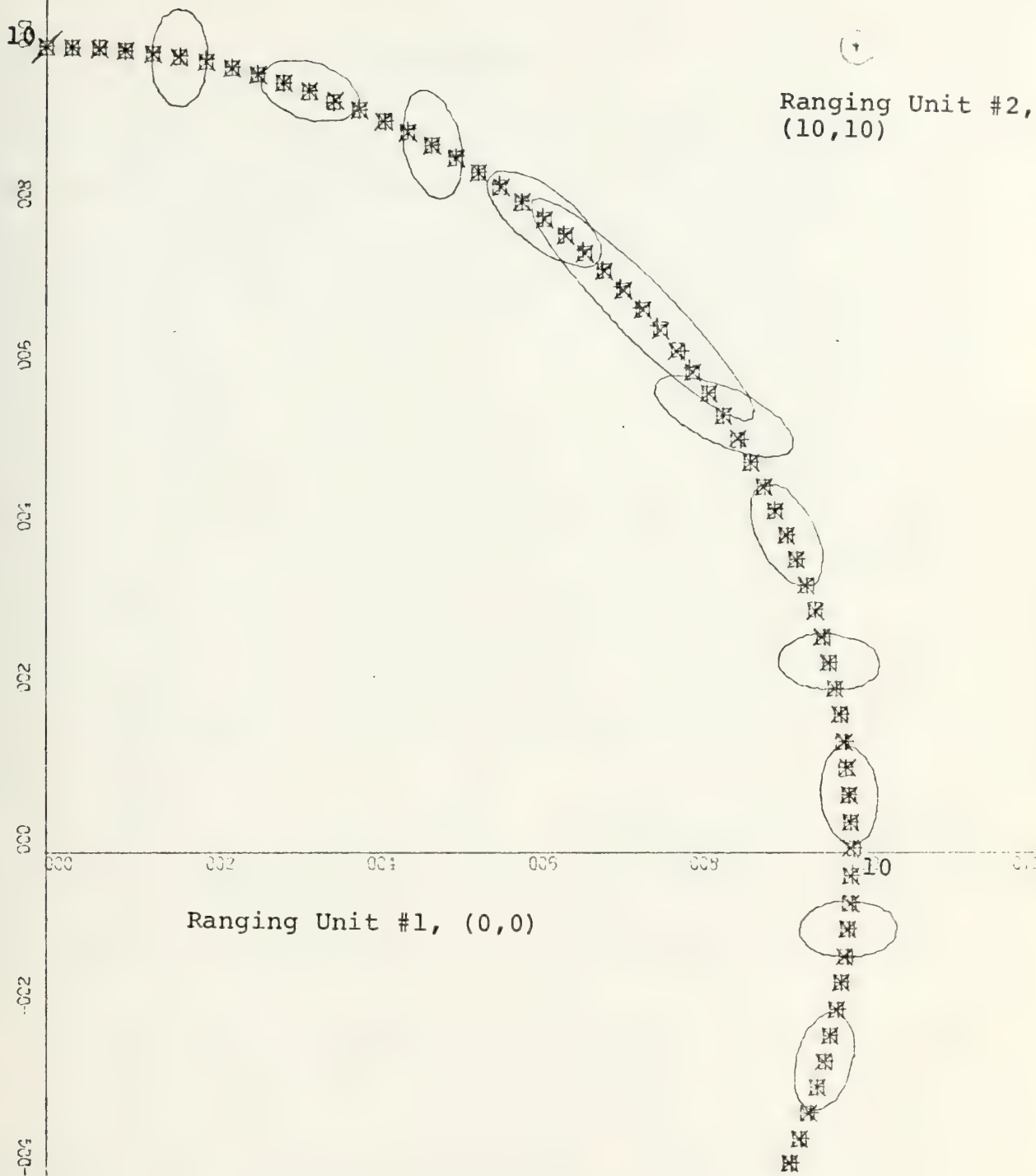


FIGURE 11. Aircraft in circular track at Mach 1 and radius of 10 KM. Switching algorithm corrected. Ellipses 20 times true scale.  
x = true track, o = noise track, + = filter track





## V. CONCLUSIONS

The evolution of this filter design appears to have some merit. The maneuvering target can be tracked handily with adequate choice of  $Q$ . The filter operated well in all but impossible ranging noise situations. The real system has range noise on the order of ten meters. The filter tracked well with a range noise sigma of one hundred meters.

The algorithm for choosing which unit to link to for ranging is finally operating satisfactorily. In fact, this may be the real contribution of this work. Another possible benefit is the use of graphical presentation of the error ellipsoids in filter evaluation. They were most essential in the algorithm for choosing ranging links and in the  $Q$  evaluation.

Still to be accomplished are: an initialization algorithm, a spurious data gating scheme and a track deletion logic. The latter two items may be dispatched readily by letting

$$\text{Gate}(k) = 3 \sqrt{P_{11}(k/k-1) + R_{11}(k)}$$

and if a unit receives no range update. Within the gate for, say, six update sequence times, then reinitialize and start over.

The rotation and reduction of the error ellipsoids (i.e. the filter error covariance) was most instructive and gave much insight into the performance of the filter.



# FILTER FOR STATIC UNITS TRACKING

```
// EXEC FORTCLGP, REGION.GO=150K
//FORT.SYSIN DD *
REAL*4LA(8)/ 'G11 ','G12 ','G22 ','G42 ','PK11','PK22','PK33',
*PK44/
DIMENSION HI(12,12),Q(12,12),H(12,12),R(12,12),G(12,12),
&PHIT(12,12),PHI(12,12),XY(800),
&G22(800),PKK(12,12),PKKM1(12,12),G11(800)
DIMENSION PINV(12,12)
DIMENSION IREAD(10),IWRITE(10)
DIMENSION DEL(12,12),A(12,12),B(12,12),D1(12,12),D2(12,12)
DIMENSION AA(12,12),YY(12),Z(12)
DIMENSION DELT(12,12)
DIMENSION G21(800)
DIMENSION G31(800),G42(800)
DIMENSION C(12,12),D(12,12),DD(12,12)
DIMENSION XP(50),YP(60)
INTEGER*4 ITB(12)/12*0/
REAL*4 RTB(28)/28*0.0/
EQUIVALENCE (TITLE,RTB(5))
REAL*8 TITLE(12)/'X' = TRUE, '+' = FILTER, SQUARE = NOISY'/
```

THIS PROGRAM COMPUTES THE FOLLOWING KALMAN FILTER EQUATIONS

$$G(K) = P(K/K-1) * HT * (H * P(K/K-1) * HT + R)^{-1}$$

$$P(K/K) = (I - G(K) * H) * P(K/K-1)$$

$$P(K/K-1) = PHI * P(K-1/K-1) * PHIT + Q$$

Q(I,J) DEFINES THE COVARIANCE OF THE PER SAMPLE RANDOM GAUSSIAN EXCITATION OF THE PROCESS.

R(I,J) DEFINES THE RANDOM (GAUSSIAN) MEASUREMENT NOISE COVARIANCE WHICH IS ADDED TO THE OBSERVABLE SIGNALS.

HI(I,J) IS THE IDENTITY MATRIX.

II=K(THE DISCRETE POINT IN TIME-THE STAGE OF THE PROCESS)

PKK(I,J) = P(K/K), (COV ERROR AT K GIVEN K SAMPLES)

PKKM1(I,J)=P(K/K-1), (COV ERROR AT K GIVEN K-1 SAMPLES)

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC



```

C  N= NUMBER OF ROWS,      M= NO. OF COL... OBS..., ND AND MD ARE THE DIMENSIONS
C  NN=NUMBER OF ITERATIONS OF FILTER
      LD=12
      READ(5,50)N,M,ND,MD,LD,NN,DT,IWRITE
      FORMAT(6I5,1F10.4/10A4,10A4)
      WRITE(6,7777)
      FORMAT(1H1)
      WRITE(6,51)N,M,ND,MD,LD,NN,DT
      FORMAT(2X,2HN=,I5,5X,2HM=,I5,5X,3HND=,I5,5X,3HMD=,I5,5X,3HLD=,
      1I5,5X,3HNN=,I5,3HDT=,F10.4)
      CALL MREAD(R,N,N,ND,MD,IWRITE)
      WRITE(6,53)
      FORMAT(//12H MATRIX R //)
      CALL MWRITE(R,N,N,ND,MD,IWRITE)
      CALL MREAD(Q,N,N,ND,MD,IWRITE)
      WRITE(6,54)
      CALL MWRITE(Q,N,N,ND,MD,IWRITE)
      FORMAT(//12H MATRIX Q //)
      CALL MREAD(PKKM1,N,N,ND,MD,IWRITE)
      WRITE(6,55)
      FORMAT(//13H MATRIX PKKM1//)
      CALL MWRITE(PKKM1,N,N,ND,MD,IWRITE)
      XDOT2(0)=V*57.3*DT(SEC)/R#3600
      CALL MREAD(PHI,N,N,ND,MD,IWRITE)
      CALL PHIDEL(DT,N,M,A,B,PHI,DEL,D1,D2,ND,MD,LD)
      FORMAT(//13H MATRIX PHI //)
      WRITE(6,58)
      CALL MWRITE(PHI,N,N,ND,MD,IWRITE)
      CALL MREAD(H,N,N,ND,MD,IWRITE)
      WRITE(6,59)
      FORMAT(//13H MATRIX H //)
      CALL MWRITE(H,N,N,ND,MD,IWRITE)
      CALL MREAD(HI,N,N,ND,MD,IWRITE)
      WRITE(6,60)
      FORMAT(//13H MATRIX HI //)
      CALL MWRITE(HI,N,N,ND,MD,IWRITE)
      CALL PROD(HI,HI,N,N,N,D,ND,MD,LD)
      WRITE(6,7777)
      T=0.0
      L=1
      ST=0.0
      NM=0
      CLOCK=ITIME(0)*0.01
      WRITE(6,52)
      FORMAT(//12H MATRIX G //)
      ITB(1)=1
      ITB(8)=2
      ITB(9)=1

```





```

1  ITB(10)=2
   ITB(11)=4
   RTB(1)=4
   RTB(2)=4
   DO 1000 II=1,NN
     THE1=0.5*ATAN(2.*PKKM1(1,2)/(PKKM1(1,1)-PKKM1(2,2)))
     THE2=0.5*ATAN(2.*PKKM1(3,4)/(PKKM1(3,3)-PKKM1(4,4)))
     SIG2X=(PKKM1(1,1)+PKKM1(2,2))/2.+PKKM1(1,2)/SIN(2.*THE1)
     SIG2Y=(PKKM1(1,1)+PKKM1(2,2))/2.-PKKM1(1,2)/SIN(2.*THE1)
     SIG2X2=(PKKM1(3,3)+PKKM1(4,4))/2.+PKKM1(3,4)/SIN(2.*THE2)
     SIG2Y2=(PKKM1(3,3)+PKKM1(4,4))/2.-PKKM1(3,4)/SIN(2.*THE2)
     SX=(SIG2X)**.5
     SY=(SIG2Y)**.5
     PT=3.14159265/12.
     CT=COS(THE1)
     ST=SIN(THE1)
     DO 1 I=1,25
       XI=I
       XP(I)=SX*COS(PT*XI)*CT-SY*SIN(PT*XI)*ST
       YP(I)=SX*COS(PT*XI)*ST+SY*SIN(PT*XI)*CT+ 15.
       CALL DRAWP(25,XP,YP,ITB,RTB)
       SX=(SIG2X2)**.5
       SY=(SIG2Y2)**.5
       CT=COS(THE2)
       ST=SIN(THE2)
       DO 7 I=1,25
         XI=I
         XP(I)=SX*COS(PT*XI)*CT-SY*SIN(PT*XI)*ST
         YP(I)=SX*COS(PT*XI)*ST+SY*SIN(PT*XI)*CT
         IF(II.LT.NN) GO TO 2
         ITB(I)=3
         IF(II.LT.NN) GO TO 2
       2 CONTINUE
       CALL DRAWP(25,XP,YP,ITB,RTB)
       DERAD=360./(3.14159265*2.)
       THE1=DERAD*THE1
       THE2=DERAD*THE2
       WRITE(6,146) THE1,SIG2X,SIG2Y,THE2,SIG2X2,SIG2Y2
       FORMAT(9(2X,1PE12.5),/)
       R(1,1)=PKKM1(4,4)
       R(2,2)=PKKM1(2,2)
       CALL GA IN(PKK,PKKM1,Q,R,PHI,H,N,M,G,HI,ND,MD,LD)
       ST=II/L
       IF(T-ST) 20,20,21
       20 MM=MM+1
          G11(MM)=G(1,1)
          G12(MM)=G(1,2)
          G21(MM)=G(2,1)

```



```

G22(MM)=G(2,2)
XY(MM)=MM-1
WRITE(6,5)I
5 FORMAT(/20X,5HTIME=,I5)
C CALL PROD(HI,PKKM1,N,N,N,D1,ND,MD,LD)
C NOTE THAT THIS RECIPI SR DESTROYS THE INPUT MATRIX
C CALL RECIPI(N,0.000001,C1,PINV,KER,MD)
C CALL TRANS(PHI,N,N,PHIT,ND,ND)
C CALL PROD(PKK,PHIT,N,N,N,A,ND,MD,LD)
C CALL PROD(A,PINV,N,N,C,ND,MD,LD)
C CALL PROD(D,C,N,N,N,DD,ND,MD,LD)
C CALL PROD(DD,HI,N,N,N,D,ND,MD,LD)
C WRITE(6,557)
C557 FORMAT(/13H MATRIX D )
C CALL MWRITE(C,N,N,ND,MD,IWRITE)
C CALL MWRITE(A,N,N,ND,MD,IWRITE)
C CALL MWRITE(D,N,N,ND,MD,IWRITE)
C WRITE(6,555)
C555 FORMAT(/13H MATRIX PKK )
C CALL MWRITE(PKK,N,N,ND,MD,IWRITE)
C WRITE(6,55)
C CALL MWRITE(PKKM1,N,N,ND,MD,IWRITE)
C WRITE(6,556)
C556 FORMAT(/13H MATRIX PINV )
C CALL MWRITE(PINV,N,N,ND,MD,IWRITE)
C WRITE(6,99)
C99 FORMAT(/13H MATRIX G /)
C21 CALL MWRITE(G,N,N,ND,MD,IWRITE)
C CONTINUE
I=I+DT
1000 CONTINUE
MC=0
CALL SSPLIT(XY,G11,MM,MC,TITLE,O,XMIN,XMAX,YMIN,YMAX)
CALL SSPLIT(XY,G21,MM,MC,TITLE,O,XMIN,XMAX,YMIN,YMAX)
END
SUBROUTINE SSPLIT(X,Y,N,MC,TITLE,ISC,XMIN,XMAX,YMIN,YMAX)
DIMENSION X(1),Y(1),GRID(33,81),XS(9),YS(9),TITLE(16)
INTEGER*4 GRID,BLANK/' ',DOT/'.',PLUS/'+',*,'*',#,'#',
*,'&','/
*6,7
IF(MC-1)1,1,15
1 NC=4
IF(ISC)13,13,14
13 XMAX=-1.0E+20
XMIN=-XMAX
YMAX=XMAX
YMIN=-XMAX
DO 11 I=1,N
IF(X(I)-XMAX)3,3,2

```



```

2  XMAX=X(I)
3  YXMAX=Y(I)
4  IF(X(I)-XMIN)4,4,5
5  XMIN=X(I)
6  YXMIN=Y(I)
7  IF(Y(I)-YMAX)7,7,6
8  YMAX=Y(I)
9  XYMAX=X(I)
10 IF(Y(I)-YMIN)8,8,11
11 YMIN=Y(I)
12 XYMIN=X(I)
13 CONTINUE
14 IERR=0
15 IF(MC-1)32,32,21
16 NC=NC+4
17 DO 31 I=1,N
18 IF(X(I)-XMAX)23,23,22
19 X(I)=XMAX
20 IERR=IERR+1
21 GO TO 25
22 IF(X(I)-XMIN)24,25,25
23 X(I)=XMIN
24 IERR=IERR+1
25 IF(Y(I)-YMAX)27,27,26
26 Y(I)=YMAX
27 IERR=IERR+1
28 GO TO 31
29 IF(Y(I)-YMIN)28,31,31
30 Y(I)=YMIN
31 IERR=IERR+1
32 CONTINUE
33 IF(MC-2)33,71,71
34 XR=XMAX-XMIN
35 YR=YMAX-YMIN
36 DO 41 K=1,81
37 DO 41 I=1,33
38 GRID(I,K)=BLANK
39 XTEST=XMAX*XMIN
40 YTEST=YMAX*YMIN
41 IF(XTEST)51,51,61
42 IYAXIS=80.0*(-XMIN)/XR+1.5
43 DO 52 I=1,33
44 GRID(I,IYAXIS)=DOT
45 IF(YTEST)62,62,71
46 IXAXIS=32.0*YMAX/YR+1.5
47 DO 63 J=1,81
48 GRID(IXAXIS,J)=DOT
49 CONTINUE

```





```

72 IF(MC-1)72,72,73
73 JSET=0
74 JSET=JSET+1
75 IF(JSET-4)75,74,74
75 JSET=1
DO 91 I=1,N
IPTX=32.0*(YMAX-Y(I))/YR+1.5
IPTX=80.0*(X(I)-XMIN)/XR+1.5
81 IF(IPTX-33)81,81,89
82 IF(IPTX-81)82,82,89
83 IF(IPTX)89,89,83
84 GRID(IPTX,IPTX)=XCHAR(JSET)
GO TO 91
91 IERR=IERR+1
CONTINUE
101 IF(MC-1)111,111,101
102 IF(MC-2)103,102,103
103 RETURN
GO TO 151
111 XINCR=XR/8.0
YINCR=YR/8.0
XS(1)=XMIN
YS(1)=YMAX
DO 121 I=2,9
XS(I)=XS(I-1)+XINCR
121 DO 122 I=2,9
YS(I)=YS(I-1)-YINCR
122 IF(MC-1)151,102,131
131 IF(MC-2)102,102,151
151 PRINT 80
PRINT 10,(XS(I),I=1,9)
II=1
I=0
DO 201 IK=1,33
IF(I)161,161,162
161 PRINT 20,YS(II),(GRID(IK,IX),IX=1,81),YS(II)
II=II+1
GO TO 165
162 PRINT 30,(GRID(IK,IX),IX=1,81)
165 I=I+1
IF(I-4)201,171,171
171 I=0
201 CONTINUE
PRINT 40,(XS(I),I=1,9)
PRINT 90,(TITLE(I),I=1,NC)
IF(IERR)211,211,202
202 PRINT 50,IERR

```



```

211 IF(ISC)212,212,102
212 PRINT 60,YMAX,XYMAX,YMIN,XYMIN
PRINT 70,XMAX,YXMAX,XMIN,YXMIN
RETURN
10 FORMAT(11X,1PE9.2,8(1X,E9.2)/13X,2H**,8(10H+*****),3H+**)
20 FORMAT(1X,1PE10.3,2X,1H+,1X,81A1,1X,1H+2X,E10.3)
30 FORMAT(13X,1H*,1X,81A1,1X,1H*)
40 FORMAT(13X,2H**,8(10H+*****),3H+**/11X,1PE9.2,8(1X,E9.2))
50 FORMAT(1X,NUMBER OF POINTS OUT OF RANGE=,I4)
60 FORMAT(1X,MAX Y=,1PE12.4,AT X=,E12.4,10X,MIN Y=,E12.4,AT X=
,E12.4)
70 FORMAT(1X,MAX X=,1PE12.4,AT Y=,E12.4,10X,MIN X=,E12.4,AT Y=
,E12.4)
80 FORMAT(1H1)
90 FORMAT(1X,4A4,4H=,4A4,4H=,4A4,4H=,4A4,4H=)
END
SUBROUTINE PHIDEL(T,N,M,A,B,PHI,DEL,D1,D2,ND,MD,LD)
DIMENSION A(12,12),B(12,12),PHI(12,12),DEL(12,12),TERM(12,12),
1COR(12,12),C(12,12),D1(12,12),D2(12,12),TEIL(12,12)
TEST=1.E-7
F=1.
DO 10 IR=1,N
DO 10 IC=1,N
PHI(IR,IC)=0.
PHI(IR,IR)=1.
C(IR,IC)=A(IR,IC)
TEIL(IR,IC)=T/2.00*PHI(IR,IC)
TERM(IR,IC)=T*PHI(IR,IC)
10 DO 11 IR=1,N
DO 11 IC=1,N
COR(IR,IC)=T/F*C(IR,IC)
PHI(IR,IC)=PHI(IR,IC)+COR(IR,IC)
TEIL(IR,IC)=TEIL(IR,IC)+T/(F+1.
) * COR(IR,IC)
11 TERM(IR,IC)=TERM(IR,IC)+ T/(F+1.
)*(F+2.
)*COR(IR,IC)
12 DO 12 K=1,N
C(IR,IC)=C(IR,IC)+A(IR,K)*COR(K,IC)
F=F+1.
DO 13 IR=1,N
DO 13 IC=1,N
IF(ABS(COR(IR,IC)).GT.TEST*ABS(PHI(IR,IC))) GO TO 50
13 CONTINUE
CALL PROD(TERM,B,N,N,M,DEL,ND,MD,LD)
CALL PROD(TEIL,B,N,N,M,D2,ND,MD,LD)
DO 14 IR=1,N
DO 14 IC=1,M

```



```

14 D1(IR,IC)=DEL(IR,IC)-D2(IR,IC)
RETURN
END
THIS SUBROUTINE COMPUTES THE OPTIMUM GAIN MATRIX AND THE ERROR
COVARIANCE
SUBROUTINE GAIN(PKK,PKKM1,Q,R,PHI,H,N,M,G,HI,ND,MD,LD)
ODIMENSION PKK(12,12),Q(12,12),H(12,12),HI(12,12)
1 G(12,12),R(12,12),PHI(12,12),PHIT(12,12),TEMP(12,12),TEMP2(12,12)
2 TEMPI(12,12),PKKM1(12,12)
G(K) = P(K/K-1)*HI*(H*P(K/K-1)*HI + R)
CALL TRANS(H,N,N,HI,ND,MD)
CALL PROD(PKKM1,HI,N,N,TEMP,ND,MD,LD)
CALL PROD(H,TEMP,N,N,TEMPI,ND,MD,LD)
CALL ADD(TEMPI,R,N,N,TEMPI,ND,MD)
CALL RECIP(M,0.000001,TEMPI,TEMP2,KER,MD)
IF (KER-2) 101,110,101
110 WRITE(6,111)
111 FORMAT(5HKER=2)
101 CALL PROD(TEMP,TEMP2,N,N,G,ND,MD,LD)
NOTE HERE PKK(I,J) = P(K/K) WHERE
P(K/K) = (I-G(K)*H)*P(K/K-1)
CALL PROD(G,H,N,N,TEMP,ND,MD,LD)
DO 108 I=1,N
DO 108 J=1,N
TEMP(I,J)=TEMP(I,J)
CALL ADD(HI,TEMP,N,N,TEMP,ND,MD)
CALL PROD(TEMP,PKKM1,N,N,P(K/K-1),ND,MD,LD)
NOTE HERE PKKM1(I,J) = P(K/K-1) WHERE
P(K/K-1) = PHI*P(K-1/K-1)*PHIT + Q
CALL TRANS(PHI,N,N,PHIT,ND,MD)
CALL PROD(PKK,PHIT,N,N,TEMP,ND,MD,LD)
CALL PROD(PHI,TEMP,N,N,TEMPI,ND,MD,LD)
CALL ADD(TEMPI,Q,N,N,PKKM1,ND,MD)
RETURN
END
SUBROUTINE ADD (A,B,N,M,C,ND,MD)
DIMENSION A(ND,MD),B(ND,MD),C(ND,MD)
DO 152 I=1,N
DO 152 J=1,M
C(I,J) = A(I,J) + B(I,J)
RETURN
END
SUBROUTINE SUB (A,B,N,M,C,ND,MD)
DIMENSION A(ND,MD),B(ND,MD),C(ND,MD)
DO 152 I=1,N
DO 152 J=1,M
C(I,J) = A(I,J) - B(I,J)
RETURN
END

```

01  
02  
03  
04  
05  
5A  
06  
07  
08  
09  
10  
11



```

END
SUBROUTINE PROD (A,B,N,M,L,C,ND,MD,LD)
DIMENSION A(ND,MD),B(MD,LD),C(ND,LD)
DO 1 I=1,ND
DO 1 J=1,LD
1 C(I,J)=0.
DO 151 I=1,N
DO 151 J=1,L
DO 151 K=1,M
151 C(I,J) = C(I,J) + A(I,K)*B(K,J)
END
SUBROUTINE TRANS(A,N,M,C,ND,MD)
DIMENSION A(ND,MD),C(MD,ND)
DO 153 I=1,N
DO 153 J=1,M
153 C(J,I) = A(I,J)
END
SUBROUTINE CONST(Q,A,N,M,C,ND,MD)
DIMENSION A(ND,MD),C(ND,MD)
IF(Q)11,10,11
10 DO 100 I=1,N
DO 100 J=1,M
100 C(I,J) = 0.0
END
11 IF(Q-1.0)13,12,13
12 DO 120 I=1,N
DO 120 J=1,M
120 C(I,J) = A(I,J)
END
13 IF(Q+1.0)15,14,15
14 DO 140 I=1,N
DO 140 J=1,M
140 C(I,J) = -A(I,J)
END
15 DO 150 I=1,N
DO 150 J=1,M
150 C(I,J) = Q*A(I,J)
END
SUBROUTINE RECIP(N,EP,B,X,KER,M)
DIMENSION A(12,12),X(M,M),B(M,M)
CALL CONST(1.,B,N,N,A,12,12)
DO 1 J=1,M
DO 1 I=1,M
1 X(I,J)=0.
DO 1 X(I,J)=1,N

```

```

12
13
14A
14B
14C
15
16
18
19A
20
21
22
23
24
25
26
27
28
30
31
32
33
35
36
37
38
40
41
42
43
44
45
46
47
000040
000050

```





000060  
000070  
000080  
000090  
000100

000130  
000140  
000160  
000170  
000180  
000190  
000200  
000210  
000220  
000230

000260  
000270  
000290  
000300  
000310  
000320  
000330  
000340  
000350  
000360  
000370  
000380  
000390

000410  
000430  
000440  
000450  
000460  
000470  
000480

```

2  X(K,K)=1.
10 DO 34 L=1,N
   KP=0
   Z=0.
   DO 12 K=L,N
     IF(Z.GE.ABS(A(K,L))) GO TO 12
     Z=ABS(A(K,L))
11  KP=K
12  CONTINUE
13  IF(L.GE.KP) GO TO 20
   DO 14 J=L,N
     Z=A(L,J)
     A(L,J)=A(KP,J)
     A(KP,J)=Z
14  A(KP,J)=Z
   DO 15 J=1,N
     Z=X(L,J)
     X(L,J)=X(KP,J)
     X(KP,J)=Z
15  X(KP,J)=Z
20  IF(ABS(A(L,L)).LE.EP) GO TO 50
30  IF(L.GE.N) GO TO 34
31  LPI=L+1
   DO 36 K=LPI,N
     IF(A(K,L).EQ.0.) GO TO 36
32  RATIO=A(K,L)/A(L,L)
   DO 33 J=LPI,N
     A(K,J)=A(K,J)-RATIO*A(L,J)
33  A(K,J)=A(K,J)-RATIO*A(L,J)
   DO 35 J=1,N
     X(K,J)=X(K,J)-RATIO*X(L,J)
35  X(K,J)=X(K,J)-RATIO*X(L,J)
36  CONTINUE
34  DO 43 I=1,N
   I1=N+1-I
   DO 43 J=1,N
     S=0.
     IF(I1.GE.N) GO TO 43
41  IIP1=I1+1
     DO 42 K=IIP1,N
       S=S+A(I1,K)*X(K,J)
42  S=S+A(I1,K)*X(K,J)
43  X(I1,J)=(X(I1,J)-S)/A(I1,I1)
     KER=1
     RETURN
50  KER=2
   RETURN
END
SUBROUTINE MREAD(A,N,M,ND,MD,IREAD)
DIMENSION A(ND,MD),IREAD(10)
DO 10 I=1,N
10  READ(5,20)(A(I,J),J=1,M)

```



```

20 FORMAT(8F10.5)
RETURN
END
SUBROUTINE MWRITE(A,N,M,ND,MD,IWRITE)
DIMENSION A(ND,MD),IWRITE(10)
DO 10 I=1,N
DO 10 J=1,M
WRITE(6,20)(I,J,A(I,J),J=1,M)
20 FORMAT(6(3X,:(,I2,;,I2,;)= ,1PE10.3))
RETURN
END
//GO.FT06F001 DD SPACE=(CYL,(6,1))
//GO.SYSIN DD *
4 2 12 12 12 10 1.

```

0.

28.	41.52				
41.52	76.	76.	41.52	41.52	28.
1.	1.	1.	1.	1.	1.
		1.			
1.	1.	1.	1.	1.	1.



# FILTER FOR TRACKING MANEUVERING AIRCRAFT

```

// EXEC FORTCLGP, REGION.GO=200K
// FORT
C THIS PROGRAM PERFORMS MONTE CARLO SIMULATION OF STATE ESTIMATORS
C OF WHICH THE KALMAN FILTER IS ONE EXAMPLE. THERE ARE SEVERAL
C OPTIONS AVAILABLE AS INDICATED IN THE DETAILLED COMMENTS BELOW.
C IT SHOULD BE NOTED THAT ALL COMPUTATIONS OF GAINS USING THE
C SUBROUTINE GAIN ARE PERFORMED IN DOUBLE PRECISION. THUS ALL
C ARRAYS FOR USE IN "GAIN" MUST BE PREPARED ACCORDINGLY.
C
C REAL*8 GAMMA, COVM, R, PHI, H, TEMP, TEMPI, TEMP2, PKKM1, G, PKK, Q, EI
C COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVM(4,4),
C 1TEMP(4,4), TEMPI(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
C 2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,60), ERR(4,60),
C 3GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
C 4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4), Z(4), V(4), SIGV(4),
C 5XHATZ(4), XZ(60), YZ(60), PX(10), PY(10),
C 6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITR0, IXZ, IV, IW, IEST, ND
C DIMENSION XP(80), YP(80)
C
C N=ORDER OF SYSTEM MODEL AND FILTER (DIMENSION OF X,XHAT)
C M=NUMBER OF MEASUREMENTS (DIMENSION OF THE VECTOR Z)
C IN=NUMBER OF INPUT RANDOM FORCING FCNS (=DIMENSION OF W)
C NSAM=NUMBER OF TIME SAMPLES
C NENS=NUMBER OF MEMBERS IN ENSEMBLE
C READ (5,81) N,M,IN,NSAM,NENS
C
C READ (5,32) ND
C THE VALUE OF ND READ IN MUST EQUAL THE ROW (AND COLUMN) DIMENSION
C SPECIFIED FOR THE SQUARE MATRIX "TEMPI", E.G. IF TEMPI(3,3) IS
C SPECIFIED IN THE COMMON STATEMENT "ND" MUST BE EQUAL TO 3.
C
C IG=-1 -- GAINS COMPUTED OFF-LINE AND READ IN
C 0 -- GAINS COMPUTED ONLY ONCE BEFORE STARTING MONTE CARLO
C 1 -- GAINS COMPUTED FOR EACH MEMBER OF ENSEMBLE
C
C IFLR=0 -- R IS READ IN
C IFLR.NE.0 -- R IS COMPUTED ON-LINE AT EACH TIME SAMPLE
C
C IEST=0 -- STANDARD KALMAN FILTER EQUATION IS USED
C IEST.NE.0 -- STD. KALMAN FILTER EQ. NOT USED

```

MCSPO0000  
 MCSPO0001  
 MCSPO0002  
 MCSPO0003  
 MCSPO0004  
 MCSPO0005  
 MCSPO0006  
 MCSPO0007  
 MCSPO0008  
 MCSPO0009  
 MCSPO0010  
 MCSPO0011  
 MCSPO0012  
 MCSPO0014  
 MCSPO0015  
 MCSPO0016  
 MCSPO0017  
 MCSPO0018  
 MCSPO0019  
 MCSPO0020  
 MCSPO0021  
 MCSPO0022  
 MCSPO0023  
 MCSPO0024  
 MCSPO0025  
 MCSPO0026  
 MCSPO0027  
 MCSPO0028  
 MCSPO0029  
 MCSPO0030  
 MCSPO0031  
 MCSPO0032  
 MCSPO0033  
 MCSPO0034  
 MCSPO0035  
 MCSPO0036  
 MCSPO0037  
 MCSPO0038  
 MCSPO0039  
 MCSPO0040  
 MCSPO0041  
 MCSPO0042  
 MCSPO0043  
 MCSPO0044  
 MCSPO0045

CCCCCCCCCCCCCC CC CCCCCCCCCCCCCCCCCC









CCCCCCCC

```
ISIGV=0 -- STD. DEVIATIONS OF MEASUREMENT NOISE TO BE READ IN (SP) MCSP00095
ISIGW=0 -- STD. DEVIATIONS OF RANDOM INPUTS TO BE READ IN (SP) MCSP00096
IXHZ=0 -- INITIAL VALUE OF THE PREDICTED VALUE XH(0/-1) TO MCSP00097
          BE READ IN (S.P.) MCSP00098
          MCSP00099
          MCSP0100
          MCSP0101
          MCSP0107
          MCSP0108
          MCSP0109
          MCSP0110
          MCSP0111
          MCSP0112
          MCSP0113
          MCSP0114
          MCSP0115
          MCSP0116
          MCSP0117
          MCSP0118
          MCSP0119
          MCSP0120
          MCSP0121
          MCSP0122
          MCSP0123
          MCSP0124
          MCSP0125
          MCSP0126
```

```
READ (5,86) IPHI,IH,IR,IPKKM1,IGAM,ISIGV,ISIGW,IXHZ,IC
CALL OVFLOW
IW = 6395217
IV = 1936743
IXZ = 135769
```

CCCCCCC

THE FOLLOWING SECTION PRINTS OUT A DESCRIPTION OF THE RUN AS  
SPECIFIED BY THE USER'S FLAGS

```
1 WRITE (6,156)
  WRITE (6,87)
  IF (IG.EQ.0) GO TO 1
  IF (IG.EQ.1) GO TO 2
  WRITE (6,88)
  GO TO 3
2 WRITE (6,89)
  GO TO 3
3 WRITE (6,90)
  IF (IEST.EQ.0) GO TO 4
  WRITE (6,91)
  GO TO 5
4 WRITE (6,92)
  IF (ITRK.EQ.0) GO TO 8
  IF (ITRK.EQ.-1) GO TO 7
  IF (ITRO.EQ.0) GO TO 6
  WRITE (6,93)
  GO TO 9
5 WRITE (6,94)
  GO TO 9
6 WRITE (6,95)
  GO TO 9
7 WRITE (6,96)
  IF (ISTAT.EQ.0) GO TO 10
  WRITE (6,97)
  GO TO 11
8 WRITE (6,98)
  GO TO 13
9 WRITE (6,99)
  IF (IQ.EQ.0) GO TO 13
  IF (IQ.EQ.1) GO TO 12
  WRITE (6,99)
```

MCSP0129  
MCSP0130  
MCSP0131  
MCSP0132  
MCSP0133  
MCSP0134  
MCSP0135  
MCSP0136  
MCSP0137  
MCSP0138  
MCSP0139  
MCSP0140  
MCSP0141  
MCSP0142  
MCSP0143  
MCSP0144  
MCSP0145  
MCSP0146  
MCSP0147



```

12 GO TO 14 (6,100)
13 WRITE (6,101)
14 IF (IFL.R.EQ.0) GO TO 15
15 WRITE (6,102)
16 GO TO 16
17 WRITE (6,103)
18 IF (IPHI.EQ.0) WRITE (6,105)
19 IF (IPH.EQ.0) WRITE (6,106)
20 IF (IFL.R.EQ.0) WRITE (6,107)
21 IF (IQ.EQ.0) GO TO 17
22 IF (IQ.EQ.-1) GO TO 18
23 WRITE (6,108)
24 GO TO 18
25 WRITE (6,109)
26 IF (ISIGV.EQ.0) WRITE (6,110)
27 IF (ISIGW.EQ.0) WRITE (6,111)
28 IF (ISIGZ.EQ.0) WRITE (6,112)
29 IF (IC.NE.1) WRITE (6,113)
30 IF (IPKML.EQ.0) WRITE (6,114)
31 IF (IPKML.EQ.0) WRITE (6,115)

```

THE FOLLOWING SECTION PRINTS OUT A DESCRIPTION OF THE OUTPUT  
DATA CALLED FOR

```

WRITE (6,116)
IF (IPRT.NE.0) GO TO 19
WRITE (6,117)
IF (IG.EQ.0) WRITE (6,118)
WRITE (6,119)
IF (ISTAT.NE.0) WRITE (6,120)
GO TO 20
WRITE (6,121)
IF (IPT.NE.0) GO TO 21
WRITE (6,122)
IF (IGPLT.EQ.1) WRITE (6,123)
IF (ITHVPL.EQ.1) WRITE (6,124)
IF (IMTPLT.EQ.1) WRITE (6,125)
IF (ISMPLT.EQ.1) WRITE (6,126)
IF (ISVPLT.EQ.1) WRITE (6,127)
GO TO 22
WRITE (6,128)
CONTINUE
WRITE (6,156)

```

CCCCC

MCSP0148  
MCSP0149  
MCSP0150  
MCSP0151  
MCSP0152  
MCSP0153  
MCSP0154  
MCSP0155  
MCSP0156  
MCSP0157  
MCSP0158  
MCSP0159  
MCSP0160  
MCSP0161  
MCSP0162  
MCSP0163  
MCSP0164  
MCSP0165  
MCSP0166  
MCSP0167  
MCSP0168  
MCSP0169  
MCSP0170  
MCSP0171  
MCSP0172  
MCSP0173  
MCSP0174  
MCSP0175  
MCSP0176  
MCSP0177  
MCSP0178  
MCSP0179  
MCSP0180  
MCSP0181  
MCSP0182  
MCSP0183  
MCSP0184  
MCSP0185  
MCSP0186  
MCSP0187  
MCSP0188  
MCSP0189  
MCSP0190  
MCSP0191  
MCSP0192  
MCSP0193  
MCSP0194  
MCSP0195



WRITE (6,129) N,M,IN,NSAM,NENS,ND  
 WRITE (6,130) N,M,IN,NSAM,NENS,ND

THE FOLLOWING SECTION READS THE SPECIFIED INPUT MATRICES

IF (IPHI.NE.0) GO TO 24  
 CALL MREAD (PHI,N,N)

DO 23 I=1,N

DO 23 J=1,N  
 23 PHIS(I,J) = PHI(I,J)

WRITE (6,131)  
 CALL MWRITE (PHI,N,N)

24 IF (IH.NE.0) GO TO 26  
 CALL MREAD (H,M,N)

DO 25 I=1,M

DO 25 J=1,N  
 25 HS(I,J) = H(I,J)

WRITE (6,132)  
 CALL MWRITE (H,M,N)

26 IF (IR.NE.0) GO TO 27  
 CALL MREAD (R,M,M)  
 WRITE (6,133)  
 CALL MWRITE (R,M,M)

27 IF (IQ.NE.1) GO TO 28  
 CALL MREAD (COVW,IN,IN)  
 WRITE (6,134)  
 CALL MWRITE (COVW,IN,IN)  
 GO TO 29

28 IF (IQ.NE.0) GO TO 29  
 CALL MREAD (Q,N,N)  
 WRITE (6,135)  
 CALL MWRITE (Q,N,N)

29 IF (IGAM.NE.0) GO TO 31

MCSP0196  
 MCSP0197  
 MCSP0198  
 MCSP0199  
 MCSP0200  
 MCSP0201  
 MCSP0202  
 MCSP0203  
 MCSP0204  
 MCSP0205  
 MCSP0206  
 MCSP0207  
 MCSP0208  
 MCSP0209  
 MCSP0210  
 MCSP0211  
 MCSP0212  
 MCSP0213  
 MCSP0214  
 MCSP0215  
 MCSP0216  
 MCSP0217  
 MCSP0218  
 MCSP0219  
 MCSP0220  
 MCSP0221  
 MCSP0222  
 MCSP0223  
 MCSP0224  
 MCSP0225  
 MCSP0226  
 MCSP0227  
 MCSP0228  
 MCSP0229  
 MCSP0230  
 MCSP0231  
 MCSP0232  
 MCSP0233  
 MCSP0234  
 MCSP0235  
 MCSP0236  
 MCSP0237  
 MCSP0238  
 MCSP0239  
 MCSP0240  
 MCSP0241  
 MCSP0242  
 MCSP0243





```

C      CALL MREAD (GAMMA,N,IN)
C      DO 30 I=1,N
C
C      DO 30 J=1,IN
C      30 GAMMAS(I,J) = GAMMA(I,J)
C      WRITE (6,136)
C      CALL MWRITE (GAMMA,N,IN)
C
C      31 IF (IPKKM1.NE.0) GO TO 32
C      CALL MREAD (PKKM1,N,N)
C      WRITE (6,137)
C      CALL MWRITE (PKKM1,N,N)
C
C      32 IF (ISIGV.NE.0) GO TO 33
C      CALL VREAD (SIGV,M)
C      WRITE (6,138)
C      CALL VWRITE (SIGV,M)
C
C      33 IF (ISIGW.NE.0) GO TO 34
C      CALL VREAD (SIGW,IN)
C      WRITE (6,139)
C      CALL VWRITE (SIGW,IN)
C
C      34 IF (IXHZ.NE.0) GO TO 35
C      CALL VREAD (XHATZ,N)
C      WRITE (6,140)
C      CALL VWRITE (XHATZ,N)
C
C      35 IF (IC.EQ.1) GO TO 36
C      IC.NE.1 MEANS THAT MEANS AND STD. DEVIATIONS OF THE INITIAL STATE
C      VALUE MUST BE READ IN. OTHERWISE NOT READ IN.
C      CALL VREAD (XZMEAN,N)
C      WRITE (6,141)
C      CALL VWRITE (XZMEAN,N)
C
C      CALL VREAD (SIGXZ,N)
C      WRITE (6,142)
C      CALL VWRITE (SIGXZ,N)
C      GO TO 40
C

```

```

MCSP0244
MCSP0245
MCSP0246
MCSP0247
MCSP0248
MCSP0249
MCSP0250
MCSP0251
MCSP0252
MCSP0253
MCSP0254
MCSP0255
MCSP0256
MCSP0257
MCSP0258
MCSP0259
MCSP0260
MCSP0261
MCSP0262
MCSP0263
MCSP0264
MCSP0265
MCSP0266
MCSP0267
MCSP0268
MCSP0269
MCSP0270
MCSP0271
MCSP0272
MCSP0273
MCSP0274
MCSP0275
MCSP0276
MCSP0277
MCSP0278
MCSP0279
MCSP0280
MCSP0281
MCSP0282
MCSP0283
MCSP0284
MCSP0285
MCSP0286
MCSP0287
MCSP0288
MCSP0289
MCSP0290
MCSP0291

```



MCSP0292  
MCSP0293  
MCSP0294  
MCSP0295  
MCSP0296  
MCSP0297  
MCSP0298  
MCSP0299  
MCSP0300  
MCSP0301  
MCSP0302  
MCSP0303  
MCSP0304  
MCSP0305  
MCSP0306  
MCSP0307  
MCSP0308  
MCSP0309  
MCSP0310  
MCSP0311  
MCSP0312  
MCSP0313  
MCSP0314  
MCSP0315  
MCSP0316  
MCSP0317  
MCSP0318  
MCSP0319  
MCSP0320  
MCSP0321  
MCSP0322  
MCSP0323  
MCSP0324  
MCSP0325  
MCSP0326  
MCSP0327  
MCSP0328  
MCSP0329  
MCSP0330  
MCSP0331  
MCSP0332  
MCSP0333  
MCSP0334  
MCSP0335  
MCSP0336  
MCSP0337  
MCSP0338  
MCSP0339

```

36 READ (5,144) (XS(I,1),I=1,N)
   INITIAL CONDITION HAS BEEN READ
   WRITE (6,143) (XS(I,1),I=1,N)
   IF (ITRK.NE.1) GO TO 40
   IF (ITRU.NE.0) GO TO 38

37 DO 37 K=2,NSAM
   READ (5,144) (XS(I,K),I=1,N)
   GO TO 39

38 CALL TRACK
   IF TRACK CALLED HERE IT SHOULD BE WRITTEN TO GENERATE AND
   STORE THE TRACK IN XS(N,K) FOR K=2(NSAM),NSAM

39 WRITE (6,145) (XS(I,1),I=1,N)
   WRITE (6,146) (XS(I,NSAM),I=1,N)
   GO CONTINUE

   THE FOLLOWING SECTION PREPARES FOR THE MONTE CARLO LOOP
   FORM NXN IDENTITY MATRIX IN DOUBLE PRECISION

   DO 41 I=1,N
   DO 41 J=1,N
   EI(I,J) = 0. DO
   IF (I.EQ.J) EI(I,J)=1. DO

41 GIVEN THE MATRIX GAMMA AND THE COVARIANCE OF W COMPUTE Q
   USING DOUBLE PRECISION ARITHMETIC
   IF (IQ.NE.1) GO TO 42
   CALL QMAT
   WRITE (6,135)
   CALL MWWRITE(Q,N,N)
   IF (IG.NE.-1) GO TO 44

42 DO 43 K=1,NSAM

   DO 43 I=1,N
   DO 43 J=1,N
   GK(I,J,K) = 1. DO

43 READ (5,144) (GK(I,J,K),J=1,M)

   GO TO 47

44 IF (IG.NE.0) GO TO 47

```



```

C      DO 46 K=1,NSAM
C      CALL GAIN
C
C      DO 46 I=1,N
C
C      DO 45 L=1,N
C      PKKS(I,L,K) = PKK(I,L)
C
C      DO 46 J=1,M
C      GKS(I,J,K) = G(I,J)
C
C      47 CONTINUE
C      IF GAINS WERE TO BE READ IN (IG=-1) OR COMPUTED ONLY
C      ONCE(IG=0), THIS HAS NOW BEEN DONE
C
C      SET UP ARRAYS FOR COMPUTING STATISTICS
C
C      DC 48 K=1,NSAM
C
C      DO 48 J=1,N
C      XM(J,K) = 0.
C      ERR(J,K) = 0.
C
C      DO 48 L=1,N
C      VAR(J,L,K) = 0.
C
C      BEGIN MAIN ITERATION LOOP HERE
C
C      DC 54 ITER=1,NENS
C      IF (IC.EQ.1) GO TO 49
C      CALL XZERO
C
C      49 DO 50 I=1,N
C      50 XHKKM1(I) = XHATZ(I)
C
C      DO 54 K=1,NSAM
C      FORM NOISY MEASUREMENT FROM TRUE STATE VALUE
C
C      DO 51 I=1,N
C      51 X(I) = XS(I,K)
C      CALL MEAS

```

MC SP0340  
 MC SP0341  
 MC SP0342  
 MC SP0343  
 MC SP0344  
 MC SP0345  
 MC SP0346  
 MC SP0347  
 MC SP0348  
 MC SP0349  
 MC SP0350  
 MC SP0351  
 MC SP0352  
 MC SP0353  
 MC SP0354  
 MC SP0355  
 MC SP0356  
 MC SP0357  
 MC SP0358  
 MC SP0359  
 MC SP0360  
 MC SP0361  
 MC SP0362  
 MC SP0363  
 MC SP0364  
 MC SP0365  
 MC SP0366  
 MC SP0367  
 MC SP0368  
 MC SP0369  
 MC SP0370  
 MC SP0371  
 MC SP0372  
 MC SP0373  
 MC SP0374  
 MC SP0375  
 MC SP0376  
 MC SP0377  
 MC SP0378  
 MC SP0379  
 MC SP0380  
 MC SP0381  
 MC SP0382  
 MC SP0383  
 MC SP0384  
 MC SP0385  
 MC SP0386  
 MC SP0387





```

C      GAIN IS NOT TO BE COMPUTED ON-LINE IF IG.NE.1
C      IF (IG.NE.1) GO TO 53
C
C      Q IS TO BE COMPUTED ON-LINE IF IFLQ.NE.0
C      IF (IFLQ.NE.0) CALL QON
C      R IS TO BE COMPUTED ON-LINE IF IFLR.NE.0
C
C      IF (IFLR.NE.0) CALL RON
C      CALL GAIN
C
C      DO 52 I=1,N
C
C      DO 52 J=1,M
C      52 GKS(I,J,K) = G(I,J)
C
C      UPDATE THE STATE ESTIMATE
C
C      53 CALL ESTIM
C
C      UPDATE RUNNING SUMS USED IN COMPUTING STATISTICS
C      CALL STAT
C      IF (K.EQ.NSAM) GO TO 54
C
C      UPDATE TRACK BY COMPUTING X(K+1)
C      IF (ITRK.NE.1) CALL TRACK
C      54 CONTINUE
C
C      DIVIDE RUNNING SUMS COMPUTED BY SUBROUTINE STAT BY ENSEMBLE
C      SIZE TO COMPUTE STATISTICS
C      ENS = NENS
C
C      DO 56 K=1,NSAM
C
C      DO 56 J=1,N
C      IF (ITRK.EQ.1) GO TO 55
C      XM(J,K) = XM(J,K)/ENS
C      55 ERR(J,K) = ERR(J,K)/ENS
C      56 VAR(J,J,K) = VAR(J,J,K)/ENS-ERR(J,K)**2
C
C      IF (ISTAT.EQ.0) GO TO 58
C
C      COMPUTE OFF-DIAGONAL TERMS IN COVARIANCE OF ESTIMATION
C      ERROR MATRIX IF ISTAT.NE.0
C      DO 57 K=1,NSAM

```

```

MC SP0388
MC SP0389
MC SP0390
MC SP0391
MC SP0392
MC SP0393
MC SP0394
MC SP0395
MC SP0396
MC SP0397
MC SP0398
MC SP0399
MC SP0400
MC SP0401
MC SP0402
MC SP0403
MC SP0404
MC SP0405
MC SP0406
MC SP0407
MC SP0408
MC SP0409
MC SP0410
MC SP0411
MC SP0412
MC SP0413
MC SP0414
MC SP0415
MC SP0416
MC SP0417
MC SP0418
MC SP0419
MC SP0420
MC SP0421
MC SP0422
MC SP0423
MC SP0424
MC SP0425
MC SP0426
MC SP0427
MC SP0428
MC SP0429
MC SP0430
MC SP0431
MC SP0432
MC SP0433
MC SP0434
MC SP0435

```



```

C      DO 57 L=2,N
      LM1 = L-1
      MCSP0436
      MCSP0437
      MCSP0438
      MCSP0439
      MCSP0440
      MCSP0441
      MCSP0442
      MCSP0443
      MCSP0444
      MCSP0445
      DO 57 J=1,LM1
      57 VAR(L,J,K) = VAR(L,J,K)/ENS-ERR(L,K)*ERR(J,K)
      MCSP0489
      MCSP0490
      58 CONTINUE
      IF (IPRT.NE.0) GO TO 64
      CALL PRT
      64 IF (IPLT.NE.0) GO TO 80
      CALL PLT
      80 CONTINUE
      STOP
      C
      81 FORMAT (5(I10))
      82 FORMAT (I2)
      83 FORMAT (7(I10))
      84 FORMAT (2(I15))
      85 FORMAT (5(I10))
      86 FORMAT (9I5)
      87 FORMAT (20X,'DESCRIPTION OF RUN',//)
      88 FORMAT (10X,'GAINS COMPUTED OFF-LINE AND READ IN',//)
      89 FORMAT (10X,'GAINS COMPUTED ONCE IN "GAIN" BEFORE STARTING MONTE CARLO',//)
      90 FORMAT (10X,'GAINS COMPUTED FOR EACH MEMBER OF ENSEMBLE',//)
      91 FORMAT (10X,'THE STANDARD LINEAR EQS. DO NOT CHARACTERIZE THE FILTER',//)
      92 FORMAT (10X,'THE STD. KALMAN EQS. CHARACTERIZE THE LINEAR FILTER',//)
      93 FORMAT (10X,'ONLY ONE TRACK IS USED AND IT IS GENERATED BY SUBROUTINE TRACK',//)
      94 FORMAT (10X,'ONLY ONE TRACK IS USED AND IT IS READ IN',//)
      95 FORMAT (10X,'SEVERAL TRACKS USED BUT NOT GENERATED FROM STD. LINEAR DIFFERENCE EQS.',//)
      96 FORMAT (10X,'SEVERAL TRACKS GENERATED BY USING THE STD. LINEAR DIFFERENCE EQS.',//)
      97 FORMAT (10X,'MEAN OF TRACK, MEAN OF EST. ERROR AND COVARIANCE OF EST. ERROR ARE COMPUTED',//)
      98 FORMAT (10X,'MEAN OF TRACK, MEAN AND VARIANCES OF EST. ERROR ARE COMPUTED',//)
      99 FORMAT (10X,'THE Q MATRIX IS COMPUTED ON-LINE AT EACH SAMPLE BY "QMCON"',//)
      100 FORMAT (10X,'THE COVARIANCE OF W IS READ IN AND Q IS COMPUTED BY "IQMAT" BEFORE STARTING MONTE CARLO',//)
      101 FORMAT (10X,'THE Q MATRIX IS READ IN',//)
      MCSP0552
      MCSP0553
      MCSP0554
      MCSP0555
      MCSP0556
      MCSP0557
      MCSP0558
      MCSP0560
      MCSP0561
      MCSP0562
      MCSP0563
      MCSP0564
      MCSP0565
      MCSP0566
      MCSP0567
      MCSP0568
      MCSP0569
      MCSP0570
      MCSP0571
      MCSP0572
      MCSP0573
      MCSP0574
      MCSP0575
      MCSP0576
      MCSP0577
      MCSP0578
      MCSP0579
      MCSP0580
      MCSP0581
      MCSP0582
      MCSP0583
      MCSP0584
      MCSP0585

```



```

102 FORMAT (10X, 'R IS COMPUTED ON-LINE AT EACH SAMPLE BY "RON",',/)
103 FORMAT (10X, 'R IS READ IN',/)
104 FORMAT (10X, '20X, 'INPUT DATA CALLED FOR',/,/)
105 FORMAT (10X, 'PHI MATRIX',/)
106 FORMAT (10X, 'H MATRIX',/)
107 FORMAT (10X, 'R MATRIX',/)
108 FORMAT (10X, 'COVARIANCE OF W',/,/)
109 FORMAT (10X, 'Q MATRIX',/)
110 FORMAT (10X, 'GAMMA MATRIX',/,/)
111 FORMAT (10X, 'STANDARD DEVIATIONS OF MEASUREMENT NOISE',/,/)
112 FORMAT (10X, 'STANDARD DEVIATIONS OF INPUT FORCING W',/,/)
113 FORMAT (10X, 'XHAT(0/-1)',/,/)
114 FORMAT (10X, 'MEANS AND VARIANCES OF X(0)',/,/)
115 FORMAT (10X, 'P(0/-1)',/,/)
116 FORMAT (10X, '20X, 'OUTPUT CALLED FOR',/,/)
117 FORMAT (10X, 'PRINTED OUTPUT OF THE FOLLOWING DATA',/,/)
118 FORMAT (15X, 'GAIN MATRICES AND THEORETICAL COVARIANCE OF EST. ERROR',/)
119 FORMAT (15X, 'SAMPLE MEANS OF TRACK AND ESTIMATION ERROR, SAMPLE VARIANCES',/)
120 FORMAT (15X, 'COVARIANCE OF ESTIMATION ERROR MATRIX',/,/)
121 FORMAT (10X, 'NO PRINTED OUTPUT CALLED FOR',/,/)
122 FORMAT (10X, 'THE FOLLOWING PLOTS ARE CALLED FOR',/,/)
123 FORMAT (15X, 'G(K) VS. K',/,/)
124 FORMAT (15X, 'P(K/K) THEORETICAL VS. K',/,/)
125 FORMAT (15X, 'MEAN OF TRACK VS. K',/,/)
126 FORMAT (15X, 'SAMPLE MEANS OF ESTIMATION ERROR VS. K',/,/)
127 FORMAT (15X, 'SAMPLE VARIANCES OF ESTIMATION ERROR VS. K',/,/)
128 FORMAT (10X, 'NO PLOTS CALLED FOR',/,/)
129 FORMAT (20X, 'INPUT DATA',/,/)
130 FORMAT (4X, 'N=', 12, 4X, 'IN=', 12, 4X, 'NSAM=', 13, 4X, 'NENS=', 12, 4X, 'ND=', 12, 4X, 'ND=')
131 FORMAT (10X, 'PHI MATRIX IS',/,/)
132 FORMAT (10X, 'H MATRIX IS',/,/)
133 FORMAT (10X, 'R MATRIX IS',/,/)
134 FORMAT (10X, 'COVARIANCE OF W MATRIX IS',/,/)
135 FORMAT (10X, 'Q MATRIX IS',/,/)
136 FORMAT (10X, 'GAMMA MATRIX IS',/,/)
137 FORMAT (10X, 'MATRIX P(0/-1) IS',/,/)
138 FORMAT (10X, 'STD. DEVIATIONS OF MEASUREMENT NOISE ARE',/,/)
139 FORMAT (10X, 'STD. DEVIATIONS OF INPUT FORCING W ARE',/,/)
140 FORMAT (10X, 'VECTOR XHAT(0/-1) IS',/,/)
141 FORMAT (10X, 'MEAN OF THE VECTOR X(0) IS',/,/)
142 FORMAT (10X, 'STANDARD DEVIATIONS OF THE VECTOR X(0) ARE',/,/)
143 FORMAT (10X, 'INITIAL STATE IS',/,/)
144 FORMAT (10X, 'THE FIRST AND LAST POINTS ON THE SINGLE TRACK TO BE USED ARE',/)
145 FORMAT (10X, '4F20.0')

```

```

MCSP0586
MCSP0587
MCSP0588
MCSP0589
MCSP0590
MCSP0591
MCSP0592
MCSP0593
MCSP0594
MCSP0595
MCSP0596
MCSP0597
MCSP0598
MCSP0599
MCSP0600
MCSP0601
MCSP0602
MCSP0603
MCSP0604
MCSP0605
MCSP0606
MCSP0607
MCSP0608
MCSP0609
MCSP0610
MCSP0611
MCSP0612
MCSP0613
MCSP0614
MCSP0615
MCSP0616
MCSP0617
MCSP0618
MCSP0619
MCSP0620
MCSP0621
MCSP0622
MCSP0623
MCSP0624
MCSP0625
MCSP0626
MCSP0627
MCSP0628
MCSP0629
MCSP0630
MCSP0631
MCSP0632
MCSP0633

```





```

146 FORMAT (9(2X,1PE12.5),/)
156 FORMAT ('1')
END
SUBROUTINE QMAT

```

CCCCCCCC

THIS SUBROUTINE COMPUTES THE MATRIX Q FROM THE EQUATION

Q=GAMMA\* E(W\*WT) \* GAMMAT

DOUBLE PRECISION ARITHMETIC IS USED

```

REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,IIRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND

```

CC

```

CALL PROD (GAMMA,COVW,N,IN,IN,TEMP)
CALL TRANS (GAMMA,N,IN,TEMP1)
CALL PROD (TEMP,TEMP1,N,IN,N,Q)
RETURN
END
SUBROUTINE QON

```

CCCC

IF Q IS TO BE COMPUTED ON-LINE (IFLQ.NE.0) IT IS DONE  
IN THIS SUBROUTINE

```

REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,IIRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND

```

CCCC

THE APPROPRIATE STATEMENTS FOR COMPUTING Q ON-LINE MUST  
BE INSERTED HERE BY THE USER

```

RETURN
END
SUBROUTINE RON

```

C

MCSP0654  
MCSP0764  
MCSP0765  
MCSP0766  
MCSP0767  
MCSP0768  
MCSP0769  
MCSP0770  
MCSP0771  
MCSP0772  
MCSP0773  
MCSP0774  
MCSP0775  
MCSP0776  
MCSP0777  
MCSP0778  
  
MCSP0780  
MCSP0781  
MCSP0782  
MCSP0783  
MCSP0784  
MCSP0785  
MCSP0786  
MCSP0787  
MCSP0788  
MCSP0789  
MCSP0790  
MCSP0791  
MCSP0792  
MCSP0793  
MCSP0794  
MCSP0795  
MCSP0796  
MCSP0797  
MCSP0798  
  
MCSP0800  
MCSP0801  
MCSP0802  
MCSP0803  
MCSP0804  
MCSP0805  
MCSP0806  
MCSP0807  
MCSP0808





C C C

IF R IS TO BE COMPUTED ON-LINE (IFLR.NE.O) IT IS DONE  
IN THIS SUBROUTINE

MCSP0809  
MCSP0810  
MCSP0811  
MCSP0812  
MCSP0813  
MCSP0814  
MCSP0815  
MCSP0816  
MCSP0817

REAL\*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKML,G,PKK,Q,EI  
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),  
ITEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKML(4,4),R(4,4),PHI(4,4),  
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,60),  
3GAMMAS(4,4,4),PHIS(4,4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),  
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKMI(4),VTMP(4),Z(4),V(4),SIGV(4),  
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),  
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRD,IXZ,IV,IW,IEST,ND

C C C C

THE APPROPRIATE STATEMENTS FOR COMPUTING R CN-LINE MUST  
BE INSERTED HERE BY THE USER

RETURN

MCSP0819  
MCSP0820  
MCSP0821  
MCSP0822  
MCSP0823  
MCSP0824  
MCSP0825  
MCSP0826  
MCSP0827  
MCSP0828  
MCSP0829  
MCSP0830  
MCSP0831  
MCSP0832  
MCSP0833  
MCSP0834  
MCSP0835  
MCSP0836  
MCSP0837  
MCSP0838

SUBROUTINE STAT COMPUTES RUNNING SUMS USED IN DETERMINING THE  
THIS SUBROUTINE SAMPLE STATISTICS OF TRACK AND ESTIMATION ERRORS. IN THE DEFAULT  
OPTION (ISTAT.EQ.O) THE STATISTICS TO BE COMPUTED ARE MEAN OF  
TRACK, MEAN OF ESTIMATION ERROR AND VARIANCE OF ESTIMATION  
ERROR. IF (ISTAT.NE.O) THE OFF-DIAGONAL TERMS IN THE COVARIANCE OF  
ESTIMATION ERROR MATRIX ARE ALSO COMPUTED.  
REAL\*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKML,G,PKK,Q,EI  
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),  
ITEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKML(4,4),R(4,4),PHI(4,4),  
1VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,60),  
2GAMMAS(4,4,4),PHIS(4,4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),  
3SIGXZ(4),XZMEAN(4),XHKK(4),XHKKMI(4),VTMP(4),Z(4),V(4),SIGV(4),  
4XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),  
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),  
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRD,IXZ,IV,IW,IEST,ND

C C C C C C

IF (ITER.NE.1) GO TO 2  
IF (ITER.NE.1) GO TO 4

C

DO 1 J=1,N  
1 XM(J,K) = XS(J,K)

C

GO TO 4  
2 CONTINUE

C

DO 3 J=1,N  
3 XM(J,K) = XM(J,K)+XS(J,K)

C

4 CONTINUE

C

DC 5 J=1,N

MCSP0840  
MCSP0841  
MCSP0842  
MCSP0843  
MCSP0844  
MCSP0845  
MCSP0846  
MCSP0847  
MCSP0848  
MCSP0849  
MCSP0850  
MCSP0851  
MCSP0852  
MCSP0853  
MCSP0854  
MCSP0855  
MCSP0856



```

C      EXH(J) = XHKK(J)-XS(J,K)
C      ERR(J,K) = ERR(J,K)+EXH(J)
5      VAR(J,J,K) = VAR(J,J,K)+EXH(J)**2
C
C      IF (ISTAT.EQ.0) RETURN
C
C      DO 6 L=2,N
C      LM1 = L-1
C
C      DO 6 J=1,LM1
C      6      VAR(L,J,K) = VAR(L,J,K)+EXH(L)*EXH(J)
C      RETURN
C
C      SUBROUTINE XZERO
C      THIS SUBROUTINE GENERATES THE INITIAL STATE VALUE FROM A NORMAL
C      RANDOM NUMBER GENERATOR. IT IS ASSUMED THAT THE INITIAL STATE
C      HAS COMPONENTS THAT ARE INDEPENDENT
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),PKKS(4,4,60),XM(4,60),ERR(4,60),
C      2VAR(4,4,60),GKS(4,4,60),XS(4,60),HS(4,4),GK(4,4),SIGM(4),X(4),
C      3GAMMAS(4,4),PHIS(4,4),XHKK(4),XHKKM1(4),VTMP(4),V(4),SIGV(4),
C      4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),
C      5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
C      6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,IYRO,IXZ,IV,IW,IEST,ND
C      CALL SNORM (IXZ,X,N)
C
C      DO 1 I=1,N
C      1      XS(I,I) = SIGXZ(I)*X(I)+XZMEAN(I)
C      RETURN
C      END
C      SUBROUTINE ADD (A,B,N,M,C)
C      THIS SUBROUTINE ADDS THE NXM MATRICES A AND B, STORING THE
C      RESULT IN C
C      REAL*8 A,B,C
C      DIMENSION A(4,4),B(4,4),C(4,4)
C
C      DO 1 I=1,N
C
C      DO 1 J=1,M
C      1      C(I,J) = A(I,J)+B(I,J)
C      RETURN
C      END
C      SUBROUTINE MREAD (A,N,M)
C      8DIC.5. THE ENTRIES IN THE FIRST ROW OF A ARE READ FIRST, THEN

```



```

C      THIS SUBROUTINE READS AN NXM MATRIX A ACCORDING TO THE FORMAT
C      THE ENTRIES IN THE SECOND ROW, AND SO ON.
C      REAL*8 A
C      DIMENSION A(4,4)
C
C      DO 1 I=1,N
C      1 READ (5,2) (A(I,J),J=1,M)
C      RETURN
C
C      2 FORMAT (8F10.0)
C      END
C      SUBROUTINE MWRITE (A,N,M)
C      THIS SUBROUTINE WRITES THE ENTRIES OF THE NXM MATRIX A
C      REAL*8 A
C      DIMENSION A(4,4)
C
C      DO 1 I=1,N
C      1 WRITE (6,2) (A(I,J),J=1,M)
C      RETURN
C
C      2 FORMAT (9(2X,1PE12.5))
C      END
C      SUBROUTINE PROD (A,B,N,M,L,C)
C      THIS SUBROUTINE COMPUTES THE MATRIX PRODUCT AB AND STORES THE
C      RESULT IN C
C      A = NXM, B = MXL, C = NXL
C      REAL*8 A,B,C,T
C      DIMENSION A(4,4),B(4,4),C(4,4),T(4,4)
C
C      DO 1 I=1,N
C      DO 1 J=1,L
C      1 T(I,J) = 0.0
C
C      DO 2 I=1,N
C      DO 2 J=1,L
C      DO 2 K=1,M
C      2 T(I,J) = T(I,J)+A(I,K)*B(K,J)
C
C      DO 3 I=1,N
C      DO 3 J=1,L

```

MCSP0967  
 MCSP0969  
 MCSP0970  
 MCSP0971  
 MCSP0972  
 MCSP0973  
 MCSP0974  
 MCSP0975  
 MCSP0976  
 MCSP0977  
 MCSP0978  
 MCSP0979  
 MCSP0980  
 MCSP0981  
 MCSP0982  
 MCSP0983  
 MCSP0984  
 MCSP0985  
 MCSP0986  
 MCSP0987  
 MCSP0988  
 MCSP0989  
 MCSP0990  
 MCSP0991  
 MCSP0992  
 MCSP0993  
 MCSP0994  
 MCSP0995  
 MCSP0996  
 MCSP0997  
 MCSP0998  
 MCSP0999  
 MCSPI000  
 MCSPI001  
 MCSPI002  
 MCSPI003  
 MCSPI004  
 MCSPI005  
 MCSPI006  
 MCSPI007  
 MCSPI008  
 MCSPI009  
 MCSPI010  
 MCSPI011  
 MCSPI012  
 MCSPI013  
 MCSPI014  
 MCSPI015





```

3 C(I,J) = T(I,J)
RETURN
END
SUBROUTINE SUB (A,B,N,M,C)
THIS SUBROUTINE SUBTRACTS THE NXM MATRIX B FROM THE NXM MATRIX
A AND STORES THE RESULT IN C
REAL*8 A,B,C
DIMENSION A(4,4),B(4,4),C(4,4)
DO 1 I=1,N
DO 1 J=1,M
1 C(I,J) = A(I,J)-B(I,J)
RETURN
END
SUBROUTINE TRANS (A,N,M,C)
THIS SUBROUTINE FORMS THE MATRIX TRANSPOSE OF A STORING THE
RESULT IN C
A = NXM, C = MXN
REAL*8 A,C
DIMENSION A(4,4),C(4,4)
DO 1 I=1,N
DO 1 J=1,M
1 C(J,I) = A(I,J)
RETURN
END
SUBROUTINE VADD (X,Y,N,Z)
THIS SUBROUTINE COMPUTES THE SUM OF THE N-VECTORS X AND
Y AND STORES THE RESULT IN THE N-VECTOR Z
REAL*8 X(4),Y(4),Z(4)
DO 1 I=1,N
1 Z(I) = X(I)+Y(I)
RETURN
END
SUBROUTINE VPROD (A,X,M,N,Y)
THIS SUBROUTINE COMPUTES THE PRODUCT OF THE MXN MATRIX
A AND THE N-VECTOR X AND STORES THE RESULT IN THE
M-VECTOR Y

```



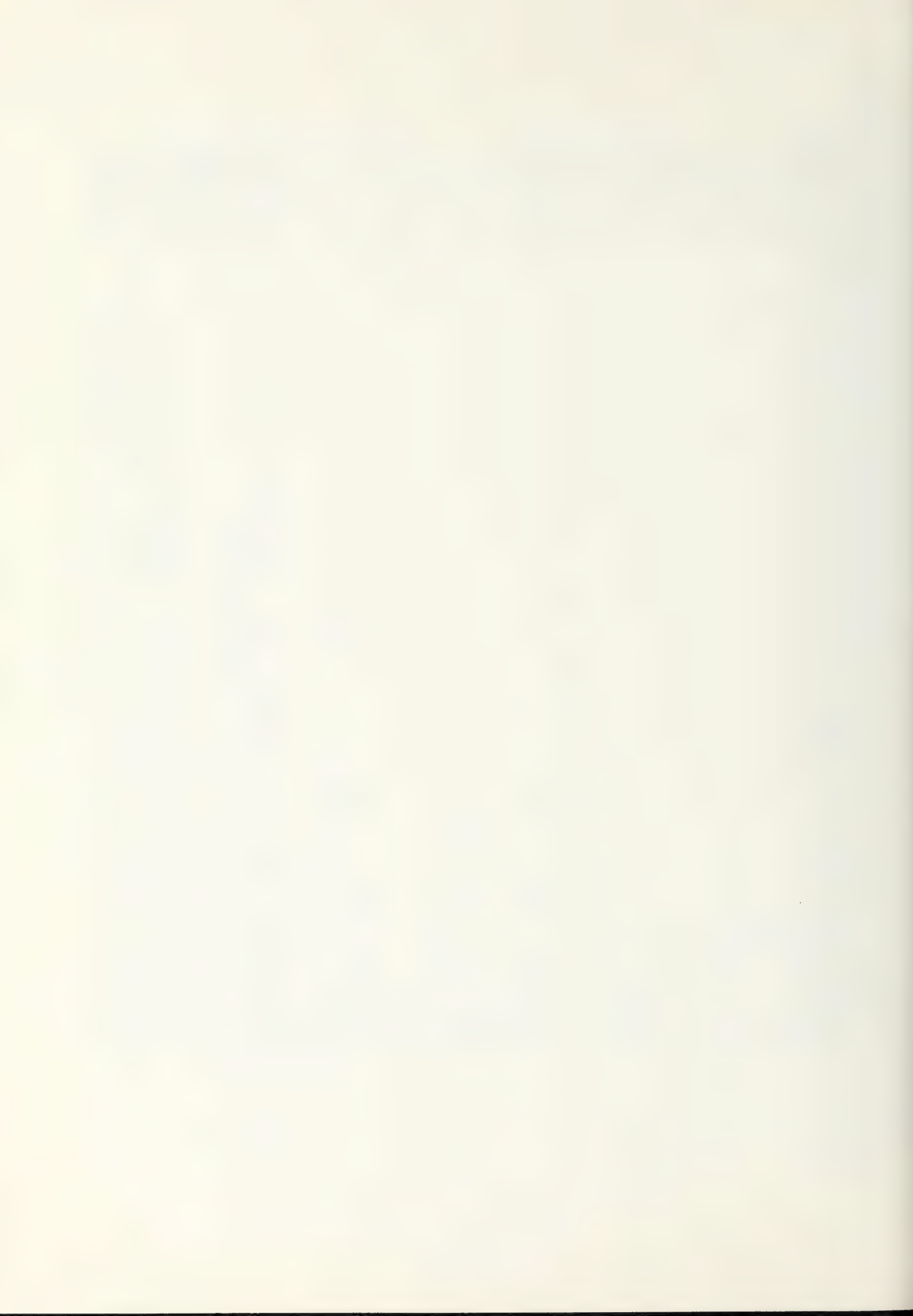
MCSP1064  
MCSP1065  
MCSP1066  
MCSP1067  
MCSP1068  
MCSP1069  
MCSP1070  
MCSP1071  
MCSP1072  
MCSP1073  
MCSP1074  
MCSP1075  
MCSP1076  
MCSP1077  
MCSP1078  
MCSP1079  
MCSP1080  
MCSP1081  
MCSP1082  
MCSP1083

```

C      REAL*4 A(4,4),X(4),Y(4),T(4)
C      DC 1 I=1,M
C      T(I) = 0.DO
C      DC 1 J=1,N
C      1 T(I) = T(I)+A(I,J)*X(J)
C      DC 2 I=1,M
C      2 Y(I) = T(I)
C      RETURN
C      END
C      SUBROUTINE VREAD (V,N)
C      THIS SUBROUTINE READS THE N-DIMENSIONAL S.P. VECTOR V
C      DIMENSION V(4)
C      READ (5,1) (V(I),I=1,N)
C      RETURN
C      1 FORMAT (8F10.0)
C      END
C      SUBROUTINE VSUB (X,Y,N,Z)
C      REAL*4 X(4),Y(4),Z(4)
C      DC 1 I=1,N
C      1 Z(I) = X(I)-Y(I)
C      RETURN
C      END
C      SUBROUTINE VWRITE (V,N)
C      DIMENSION V(4)
C      WRITE (6,1) (V(I),I=1,N)
C      RETURN
C      1 FORMAT (9(2X,1PE12.5))
C      END
C      SUBROUTINE TRACK
C      IF TRACK IS TO BE GENERATED ON-LINE IT IS DCNE IN THIS SUBROUTINE
C      IN THE DEFAULT OPTION (ITRK.EQ.0) THE TRACK IS GENERATED
C      FROM THE STANDARD LINEAR DIFFERENCE EQUATION
C      X(K+1)=PHI*X(K)+GAMMA*W(K)
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),G(4,4),GAMMA(4,4),COVW(4,4),
C      1 TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      2 VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
C      3 GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),SIGW(4),X(4),
C      4 SIGXZ(4),XZMEAN(4),XHKK(4),VTEMP(4),Z(4),V(4),SIGV(4),

```

MCSP0871  
MCSP0872  
MCSP0873  
MCSP0874  
MCSP0875  
MCSP0876  
MCSP0877  
MCSP0878  
MCSP0879  
MCSP0880  
MCSP0881  
MCSP0882  
MCSP0883



```

5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND
DIMENSION N(3)
ITRK NE.0 OR 1 -- SEVERAL TRACKS GENERATED,BUT NOT FROM STD.
= 0 -- SEVERAL TRACKS GENERATED FROM STD LINEAR EQS
= 1 -- ONLY ONE TRACK IS USED
IF (ITRK.NE.0) GO TO 4
CALL SNORM (IW,W,IN)
CCONVERT EACH N(0,1) R.V. TO N(0,SIGW(I)) R.V.

DO 1 I=1,IN
1 W(I) = SIGW(I)*W(I)

DO 2 I=1,N
2 X(I) = XS(I,K)

CALL VPROD (GAMMAS,W,N,IN,W)
CALL VPROD (PHIS,X,N,N,VTMP)
CALL VADD (VTMP,W,N,VTMP)

DO 3 I=1,N
3 XS(I,K+1) = VTMP(I)

NEW VALUE OF X HAS BEEN COMPUTED AND STORED IN THE ARRAY XS
RETURN
4 IF (ITRK.NE.1) GO TO 6
IF (ITRK.EQ.1) THE USER MUST INSERT HERE THE STATEMENTS REQUIRED
TO GENERATE A SINGLE TRAJECTORY AND STORE IT IN THE ARRAY
XS(I,K),I=1,N,K=2,NSAM (NOTE THAT IF A SINGLE TRAJECTORY IS TO BE
GENERATED, THE INITIAL CONDITION HAS BEEN READ IN AND STORED
IN XS(I,1),I=1,N)

TPI = 2.*3.14159265
DO 5 K=2,NSAM
EKM1 = K-1
T = 1.0*EKM1
A=0.03333*T
IF (A.LT.TPI) GO TO 10
FM=A/TPI
FM=MM
A = A - FM*TPI
10 CONTINUE
XS(1,K)=10.*SIN(A)
XS(2,K)=.333*COS(A)
XS(3,K)=10.*COS(A)
5 XS(4,K)=-.333*SIN(A)

```

MCSP0885  
MCSP0886  
MCSP0887  
MCSP0888  
MCSP0889  
MCSP0890  
MCSP0891  
MCSP0892  
MCSP0893  
MCSP0894  
MCSP0895  
MCSP0896  
MCSP0897  
MCSP0898  
MCSP0899  
MCSP0900  
MCSP0901  
MCSP0902  
MCSP0903  
MCSP0904  
MCSP0905  
MCSP0906  
MCSP0907  
MCSP0908  
MCSP0909  
MCSP0910  
MCSP0911  
MCSP0912  
MCSP0913  
MCSP0914  
MCSP0915  
MCSP0916  
MCSP0917  
  
MCSP0918  
MCSP0919





```

C      RETURN
C      IF CONTINUE POINT IS REACHED, ITRK NOT EQUAL 0 CR 1 INDICATING THAT
C      IF SEVERAL TRACKS ARE TO BE GENERATED, BUT NOT BY USING THE STD.
C      LINEAR DIFFERENCE EQS..THE USER MUST SUPPLY THE APPROPRIATE
C      STATEMENTS HERE.
C      RETURN
C      END
C      SUBROUTINE MEAS
C      THIS SUBROUTINE STARTS WITH THE TRUE STATE VALUE XS
C      AND ADDS ZERO-MEAN WHITE GAUSSIAN NOISE TO H*XS TO
C      GENERATE A NOISY VECTOR OF MEASUREMENTS Z.
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
C      1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,60),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
C      4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4), Z(4), V(4), SIGV(4),
C      5XHATZ(4), XZ(60), PX(10), PY(10),
C      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND
C      ALPHA = XS(3,K)
C      BETA = XS(1,K)
C      Z(1) = SQRT( ALPHA**2+BETA**2 )
C      Z(2) = ATAN2( ALPHA, BETA )
C      CALL SNCRM ( IV, V, M )
C
C      DO 1 I=1, M
C      1 V(I) = SIGV(I)*V(I)
C
C      CALL VADD (Z, V, M, Z)
C      ALPHA = Z(1)*COS(Z(2))
C      BETA = Z(1)*SIN(Z(2))
C      XZ(K)=ALPHA
C      YZ(K)=BETA
C      RETURN
C      END
C      SUBROUTINE GAIN
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
C      1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,60),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
C      4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4), Z(4), V(4), SIGV(4),
C      5XHATZ(4), XZ(60), PX(10), PY(10),
C      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND

```

MCSP0925  
 MCSP0926  
 MCSP0927  
 MCSP0928  
 MCSP0929  
 MCSP0930  
 MCSP0931  
 MCSP0932  
 MCSP0933  
 MCSP0934  
 MCSP0735  
 MCSP0736  
 MCSP0737  
 MCSP0738  
 MCSP0739  
 MCSP0740  
 MCSP0741  
 MCSP0742  
 MCSP0743  
 MCSP0744  
 MCSP0745

MCSP0747  
 MCSP0748  
 MCSP0749  
 MCSP0750  
 MCSP0751  
 MCSP0752  
 MCSP0753  
 MCSP0754  
 MCSP0755  
 MCSP0756  
 MCSP0757  
 MCSP0758  
 MCSP0759

MCSP0762  
 MCSP0763  
 MCSP0695  
 MCSP0696  
 MCSP0697  
 MCSP0698  
 MCSP0699  
 MCSP0700  
 MCSP0701  
 MCSP0703





```

C
C
C      DIMENSION BE(4),ER(4)
C      G(K) = P(K/K-1)*HT*(H*P(K/K-1)*HT + R)
C      DO 300 I=1,4
C      DO 300 J=1,4
C      PKKS(I,J,K)=PKKM1(I,J)
C      PX(1)=0.
C      PY(1)=0.
C      PX(2)=10.
C      PY(2)=10.
C      IF(DABS(PKKM1(1,1)-PKKM1(3,3)).GT.0) GO TO 11
C      PKKM1(1,1)=PKKM1(3,3)+0.000001
C      11 CONTINUE
C      THE=0.5*DATAN(2.*PKKM1(1,3)/(PKKM1(1,1)-PKKM1(3,3)))
C      IF(ABS(THE).GT.0) GO TO 10
C      THE = 0.00001
C      10 CONTINUE
C      SIG2X=(PKKM1(1,1)+PKKM1(3,3))/2.+PKKM1(1,3)/SIN(2.*THE)
C      SIG2Y=(PKKM1(1,1)+PKKM1(3,3))/2.-PKKM1(1,3)/SIN(2.*THE)
C      DO 9 IN=1,2
C      IF(ABS(XHKKM1(1)-PX(IN)).GT.0) GO TO 9
C      XHKKM1(1)=0.000001+PX(IN)
C      9 BE(IN)=ATAN(XHKKM1(3)-PY(IN))/(XHKKM1(1)-PX(IN))
C      IF(SIG2X.GE.SIG2Y) GO TO 63
C      THE=THE+3.14159265/2.
C      63 CONTINUE
C      DO 4 IN=1,2
C      ER(IN)=ABS(THE-BE(IN))
C      4 IF(ABS(COS(ER(1))).LE.ABS(COS(ER(2)))) GO TO 7
C      GO TO 8
C      IN=1
C      7 IN=2
C      8 XIN=IN
C      RR=((XHKKM1(1)-PX(IN))**2+(XHKKM1(3)-PY(IN))**2)**.5
C      146 WRITE (6,146) THE,SIG2X,SIG2Y,BE(1),BE(2),XIN,ER(1),ER(2), RR
C      FORMAT (9(2X,1PE12.5),/)
C      H(1,1)=(XHKKM1(1)-PX(IN))/RR
C      H(1,3)=(XHKKM1(3)-PY(IN))/RR
C      CALL TRANS (H,M,N,TEMP2)
C      CALL PROCD (PKKM1,TEMP2,N,M,TEMP)
C      CALL PROCD (H,TEMP,M,N,M,TEMP1)
C      CALL ADD (TEMP1,R,M,M,TEMP1)
C      IF (M.EQ.1) GO TO 2
C      MD = ND
C      CALL GAUSS3 (M,EPS,TEMP1,TEMP2,KER,MD)
C      CALL PROD (TEMP,TEMP2,N,M,M,G)
C      NOTE HERE PKK(I,J) = P(K/K) WHERE
C
C
C      MCSP0704
C      MCSP0705
C
C      MCSP0634
C
C      MCSP0706
C      MCSP0707
C      MCSP0708
C      MCSP0709
C      MCSP0710
C      MCSP0711
C      MCSP0712
C      MCSP0713
C      MCSP0714
C      MCSP0715

```



```

C      P(K/K) = (I-G(K)*H)*P(K/K-1)
C      CALL PRCD (G,H,N,M,N,TEMP)
C      CALL SUB (EI,TEMP,N,N,TEMP2)
C      CALL PRCD (TEMP2,PKKM1,N,N,N,PKK)
C
C      NOTE HERE   PKKM1(I,J) = P(K/K-1)   WHERE
C      P(K/K-1) = PHI*P(K-1/K-1)*PHIT + Q
C      CALL TRANS (PHI,N,N,TEMP2)
C      CALL PRCD (PKK,TEMP2,N,N,N,TEMP)
C      CALL PRCD (PHI,TEMP,N,N,N,TEMP1)
C      CALL ADD (TEMP1,Q,N,N,PKKM1)
C      RETURN
C
C      DO 3 I=1,N
C      3 G(I,1) = TEMP(I,1)/TEMP1(1,1)
C
C      GC TO 1
C      END
C      SUBROUTINE ESTIM
C      THIS SUBROUTINE UPDATES THE STATE ESTIMATE. IN THE DEFAULT
C      CONDITION (IEST.EQ.0) THE STANDARD EQUATIONS
C
C      XHAT(K/) = XHAT(K/K-1) + G(K) * (Z(K) - H(K) * XHAT(K/K-1))
C
C      XHAT(K+1/K) = PHI * XHAT(K/K)
C
C      ARE EVALUATED
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4), PHI(4,4),
C      1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,60), ERR(4,60),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,4), GKI(4,4), SIGW(4,4), X(4),
C      4SIGXZ(4), XZMEAN(4), XHKK(4), PX(10), PY(10),
C      5XHATZ(4), XZ(60), YZ(60), PX(10), PY(10),
C      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITR0, IXZ, IV, IW, IEST, ND
C      TAKE THE APPROPRIATE GAIN AND STORE IN THE ARRAY GK
C
C      XIN=IN
C      DO 1 I=1,N
C      DO 1 J=1,M
C      1 GK(I,J) = GKS(I,J,K)
C
C      IF (IEST.NE.0) GO TO 2
C      CALL VPROD (HS,XHKKM1,M,N,VTMP)
C      VTMP(1) = ((XHKKM1(1)-PX(IN))**2 + (XHKKM1(3)-PY(IN))**2)**.5
C      Z(1) = ((XZ(K)-PX(IN))**2 + (YZ(K)-PY(IN))**2)**.5
C      CALL VSUB (Z,VTMP,M,VTMP)

```

MCSP0716  
 MCSP0717  
 MCSP0718  
 MCSP0719  
 MCSP0720  
 MCSP0721  
 MCSP0722  
 MCSP0723  
 MCSP0724  
 MCSP0725  
 MCSP0726  
 MCSP0727  
 MCSP0728  
 MCSP0729  
 MCSP0730  
 MCSP0731  
 MCSP0732  
 MCSP0733  
 MCSP0655  
 MCSP0656  
 MCSP0657  
 MCSP0658  
 MCSP0659  
 MCSP0660  
 MCSP0661  
 MCSP0662  
 MCSP0663  
 MCSP0664  
 MCSP0665  
 MCSP0666  
 MCSP0667  
 MCSP0668  
 MCSP0669  
 MCSP0671  
 MCSP0672  
 MCSP0673  
 MCSP0675  
 MCSP0674  
 MCSP0676  
 MCSP0677  
 MCSP0678  
 MCSP0679  
 MCSP0680  
 MCSP0681



```

C      CALL VPROD (GK,VTMP,N,M,VTMP)
C      CALL VADD (XHKKM1,VTMP,N,XHKK)
C
C      XHAT(K/K) HAS BEEN COMPUTED AND STORED IN THE ARRAY XHKK
C      CALL VPROD (PHIS,XHKK,N,N,XHKKM1)
C
C      XHAT(K+1/K) HAS BEEN COMPUTED AND STORED IN THE ARRAY XHKKM1
C      RETURN
C
C      2 CCNTINUE
C      IF STANDARD EQUATIONS ARE NOT TO BE USED, THE APPROPRIATE
C      EQUATIONS MUST BE INSERTED HERE BY THE USER.
C      RETURN
C      END
C      SUBROUTINE PRT
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
C      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
C      3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),SIGW(4,4),X(4),
C      4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
C      5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
C      6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND
C      IG=0
C      ISTAT=1
C      WRITE (6,147)
C      WRITE GAINS, THEORETICAL COVARIANCES OF ESTIMATION ERROR
C      IF ONE SET OF GAINS HAS BEEN USED.
C      IF (IG.NE.0) GO TO 61
C      WRITE (6,148)
C
C      DO 59 K=1,NSAM
C      WRITE (6,149) K
C
C      DO 59 I=1,N
C      WRITE (6,146) (GKS(I,J,K),J=1,M)
C
C      WRITE (6,150)
C
C      DO 60 K=1,NSAM
C      WRITE (6,151) K
C
C      DO 60 I=1,N
C      WRITE (6,146) (PKKS(I,J,K),J=1,N)
C
C      61 WRITE (6,156)
C      WRITE (6,152)

```

MCSP0682  
MCSP0683  
MCSP0684  
MCSP0685  
MCSP0686  
MCSP0687  
MCSP0688  
MCSP0689  
MCSP0690  
MCSP0691  
MCSP0692  
MCSP0693  
MCSP0694

MCSP0878  
MCSP0879  
MCSP0880  
MCSP0881  
MCSP0882  
MCSP0883  
MCSP0885

MCSP0446  
MCSP0447  
MCSP0448  
MCSP0449  
MCSP0450  
MCSP0451  
MCSP0452  
MCSP0453  
MCSP0454  
MCSP0455  
MCSP0456  
MCSP0457  
MCSP0458  
MCSP0459  
MCSP0460  
MCSP0461  
MCSP0462  
MCSP0463  
MCSP0464  
MCSP0465  
MCSP0466  
MCSP0467  
MCSP0468  
MCSP0469





```

C      WRITE (6,153)
C      DO 62 K=1,NSAM
C      WRITE (6,155)
C
C      DO 62 I=1,N
C      WRITE (6,154) K,I,XM(I,K),ERR(I,K),VAR(I,I,K)
C
C      WRITE (6,156)
C      IF (ISTAT.EQ.0) GO TO 64
C      WRITE (6,157)
C
C      DO 63 K=1,NSAM
C      WRITE (6,158) K
C
C      DO 63 I=1,N
C      WRITE (6,146) (VAR(I,L,K),L=1,I)
C      63 CONTINUE
C
C      146 WRITE (6,156)
C      147 WFORMAT (9(2X,1PE12.5),/)
C      148 FFORMAT (1,20X,'OUTPUT DATA',/)
C      149 FFORMAT (10X,'THE GAIN MATRICES ARE',/)
C      150 FFORMAT (5X,K=1,13,'IOX',G(K)=',') COVARIANCE MATRIX IS',/
C      151 FFORMAT (1X,/,10X,'THE THEORETICAL',/)
C      152 FFORMAT (5X,K=1,13,'IOX',P(K/K)=',')
C      153 FFORMAT (15,'SAMPLE MEAN OF',T16,'VECTOR COM-',T34,'SAMPLE MEAN',
C      154 FFORMAT (15,'SAMPLE INDEX',T16,'PONENT INDEX',T34,'CF TRACK',
C      155 FFORMAT (15,'ESTIMATION ERROR',T17,'ESTIMATION ERROR',)
C      156 FFORMAT (6X,13,13X,11,10X,1PE14.7,2(6X,1PE14.7))
C      157 FFORMAT (10X,'THE SAMPLE COVARIANCE OF EST. ERROR MATRIX IS',/)
C      158 RETURN
C      END
C
C      SUBROUTINE PLT
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),PKKS(4,4,60),XM(4,60),ERR(4,60),
C      2VAR(4,4,60),GKS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
C      3GAMMAS(4,4),PHIS(4,4),XHKK(4),XHKKM1(4),VIMP(4),Z(4),SIGV(4),
C      4SIGXZ(4),XZMEAN(4),YZ(60),YP(10),PY(10),
C      5XHA TZ(4),XZ(60),ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND
C      6NDIMENSION IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND
C      DIMENSION*4 ITB(12)/12*0/
C      INTEGER*4

```

MCSP0470  
 MCSP0471  
 MCSP0472  
 MCSP0473  
 MCSP0474  
 MCSP0475  
 MCSP0476  
 MCSP0477  
 MCSP0478  
 MCSP0479  
 MCSP0480  
 MCSP0481  
 MCSP0482  
 MCSP0483  
 MCSP0484  
 MCSP0485  
 MCSP0486  
 MCSP0487  
 MCSP0488  
 MCSP0635  
 MCSP0636  
 MCSP0637  
 MCSP0638  
 MCSP0639  
 MCSP0640  
 MCSP0641  
 MCSP0642  
 MCSP0643  
 MCSP0644  
 MCSP0645  
 MCSP0646  
 MCSP0647  
 MCSP0648  
 MCSP0878  
 MCSP0879  
 MCSP0880  
 MCSP0881  
 MCSP0882  
 MCSP0883  
 MCSP0885



```

REAL#4      RTB(28)/28*0.0/
EQUIVAL     ENCE (TITLE,RTB(5))
REAL#8      TITLE(12)/X = TRUE,  + = FILTER,  SQUARE = NOISY'/
IGPLT=1
ITHVPL=1
IMPLT=1
ISVPLT=1
DC 50 K=1, NSAM
XP(K)=XM(1,K)
YP(K)=XM(3,K)
50 CALL PLOTP(XP, YP, NSAM, 0)
ITB(1)=1
ITB(2)=1
CALL DRAWP(60, XP, YP, ITB, RTB)
DC 51 K=1, NSAM
XP(K)=XS(1,K)+ERR(1,K)
YP(K)=XS(3,K)+ERR(3,K)
51 CALL PLOTP(XP, YP, NSAM, 0)
ITB(1)=2
ITB(2)=2
CALL DRAWP(60, XP, YP, ITB, RTB)
ITB(2)=0
DC 2 J=1, 60, 5
IF (ABS(PKKS(1, 1, J)-PKKS(3, 3, J)).GT.0) GO TO 11
PKKS(1, 1, J)=PKKS(3, 3, J)+0.000001
11 CONTINUE
IF (0.5*ATAN(2.*PKKS(1, 3, J)/(PKKS(1, 1, J)-PKKS(3, 3, J)))
THE=0.000001
GO TO 10
CONTINUE
SIG2X=(PKKS(1, 1, J)+PKKS(3, 3, J))/2.+PKKS(1, 3, J)/SIN(2.*THE)
SIG2Y=(PKKS(1, 1, J)-PKKS(3, 3, J))/2.-PKKS(1, 3, J)/SIN(2.*THE)
WRITE (6, 146) THE, SIG2X, SIG2Y
146 FORMAT (9(2X, 1PE12.5), '/')
SX=(SIG2X)**.5*20.
SY=(SIG2Y)**.5*20.
PT=3.14159265/12.
CT=COS( THE )
ST=SIN( THE )
DO 1 I=1, 25
XI=1
XP(I)=SX*COS( PT*XI)*CT-SY*SIN(PT*XI)*ST+XS(1, J)
YP(I)=SX*COS( PT*XI)*ST+SY*SIN(PT*XI)*CT+ XS(3, J)
1 2 CALL DRAWP(25, XP, YP, ITB, RTB)
ITB(1)=3
ITB(2)=3
CALL DRAWP(60, XZ, YZ, ITB, RTB)

```



```

C      DO 65 K=1,NSAM
C      65 XP(K) = K
C      IF (IGPLT.NE.1) GO TO 68
C      DC 67 I=1,N
C      DO 67 J=1,M
C      DO 66 K=1,NSAM
C      66 YP(K) = GKS(I,J,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      67 WRITE (6,159) I,J
C      68 IF (ITHVPL.NE.1) GO TO 71
C      DO 70 I=1,N
C      DO 69 K=1,NSAM
C      69 YP(K) = PKKS(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      70 WRITE (6,160) I,I
C      71 IF (IMTPLT.NE.1) GO TO 74
C      DO 73 I=1,N
C      DO 72 K=1,NSAM
C      72 YP(K) = XM(I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      73 WRITE (6,161) I
C      74 IF (ISMPLT.NE.1) GO TO 77
C      DO 76 I=1,N
C      DO 75 K=1,NSAM
C      75 YP(K) = ERR(I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      76 WRITE (6,162) I,I

```

```

MCSP0491
MCSP0492
MCSP0493
MCSP0494
MCSP0495
MCSP0496
MCSP0497
MCSP0498
MCSP0499
MCSP0500
MCSP0501
MCSP0502
MCSP0503
MCSP0504
MCSP0505
MCSP0506
MCSP0507
MCSP0508
MCSP0509
MCSP0510
MCSP0511
MCSP0512
MCSP0513
MCSP0514
MCSP0515
MCSP0516
MCSP0517
MCSP0518
MCSP0519
MCSP0520
MCSP0521
MCSP0522
MCSP0523
MCSP0524
MCSP0525
MCSP0526
MCSP0527
MCSP0528
MCSP0529
MCSP0530
MCSP0531
MCSP0532
MCSP0533
MCSP0534
MCSP0535
MCSP0536
MCSP0537
MCSP0538

```



MCSP0539  
MCSP0540  
MCSP0541  
MCSP0542  
MCSP0543  
MCSP0544  
MCSP0545  
MCSP0546  
MCSP0547  
MCSP0548  
MCSP0549  
  
MCSP0550  
MCSP0551  
  
MCSP0649  
MCSP0650  
MCSP0651  
MCSP0652  
MCSP0653

```

C      77 IF (ISVPLT.NE.1) GO TO 80
C
C      DO 79 I=1,N
C
C          DO 78 K=1,NSAM
C              78 YP(K) = VAR(I,I,K)
C
C              WRITE (6,156)
C              CALL PLOTP (XP,YP,NSAM,O)
C              79 WRITE (6,163) I
C              80 CONTINUE
C
C              WRITE (6,156)
C              FORMAT ((I1))
C              156 FCFORMAT ((12X,'G(,,I1,,',I1,,)', VS.'K')
C              159 FCFORMAT ((12X,'PKK(,,I1,,',I1,,)', VS.'K')
C              160 FCFORMAT ((12X,'MEAN OF X(,,I1,,',I1,,)', VS.'K')
C              161 FCFORMAT ((12X,'XHATKK(,,I1,,',I1,,)', -X(,,I1,,)', VS.'K')
C              162 FCFORMAT ((12X,'ERROR VARIANCE(,,I1,,',I1,,)', VS..'K')
C              163 RETURN
C          END
//LINK=USDD DD DSNNAME=F0131.TITUS,UNIT=2314,DISP=SHR,

```

```

//LINK.USDD DD DSN=NAME=F0131.TITUS,UNIT=2314,DISP=SHR,

```

```
// VOLUME=SER=DUFFY
// INK.SYSIN DD *
```

INCLUDE USD(PLR)  
ENTOP MAIN

```

//GO.FTC6F001 DD SPACE=(CYL,(5,1))

```

///GU.SYSIN DD #	1	2	60	1

—

[illegible]

0.1

1.0  
1.0

0.0001  
1000.0

.0001  
1000

U  
C

0.150

1.0001	1.0001
1.0001	1.0001





.0001  
.01

0.3333

.0001

10.  
0.3333

.0001

10.



### LIST OF REFERENCES

1. H. W. Sorenson, "Kalman Filtering Techniques," Advan. Control System, Vol. 3, Chapter 5, 1966.



INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Documentation Center Cameron Station Alexandria, Virginia 22314	2
2. Library, Code 0212 Naval Postgraduate School Monterey, California 93940	2
3. Chairman, Code 52 Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	1
4. Professor H.A. Titus, Code 52Ts Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	18
5. Capt. Charles Dittmar Weapons and Systems Engineering United States Naval Academy Annapolis, Maryland	1
6. Assoc. Professor Donald E. Kirk, Code 52Ki Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	1
7. Commander Naval Electronics System Command National City Washington D.C. 22030 ATTN: Charles Gill	2
8. Marine Corps Test and Evaluation Center Camp Pendleton, California ATTN: Major Norbert Spitzer	2
9. Robert R. Fossum Dean of Research (Code 023) Naval Postgraduate School Monterey, California 93940	1









Thesis

164323

D592

Dittmar

c.1

The application of  
extended Kalman fil-  
tering to the Position  
Locating Reporting  
System (PLRS).

thesD592

The application of extended Kalman filter



3 2768 001 89421 5

DUDLEY KNOX LIBRARY